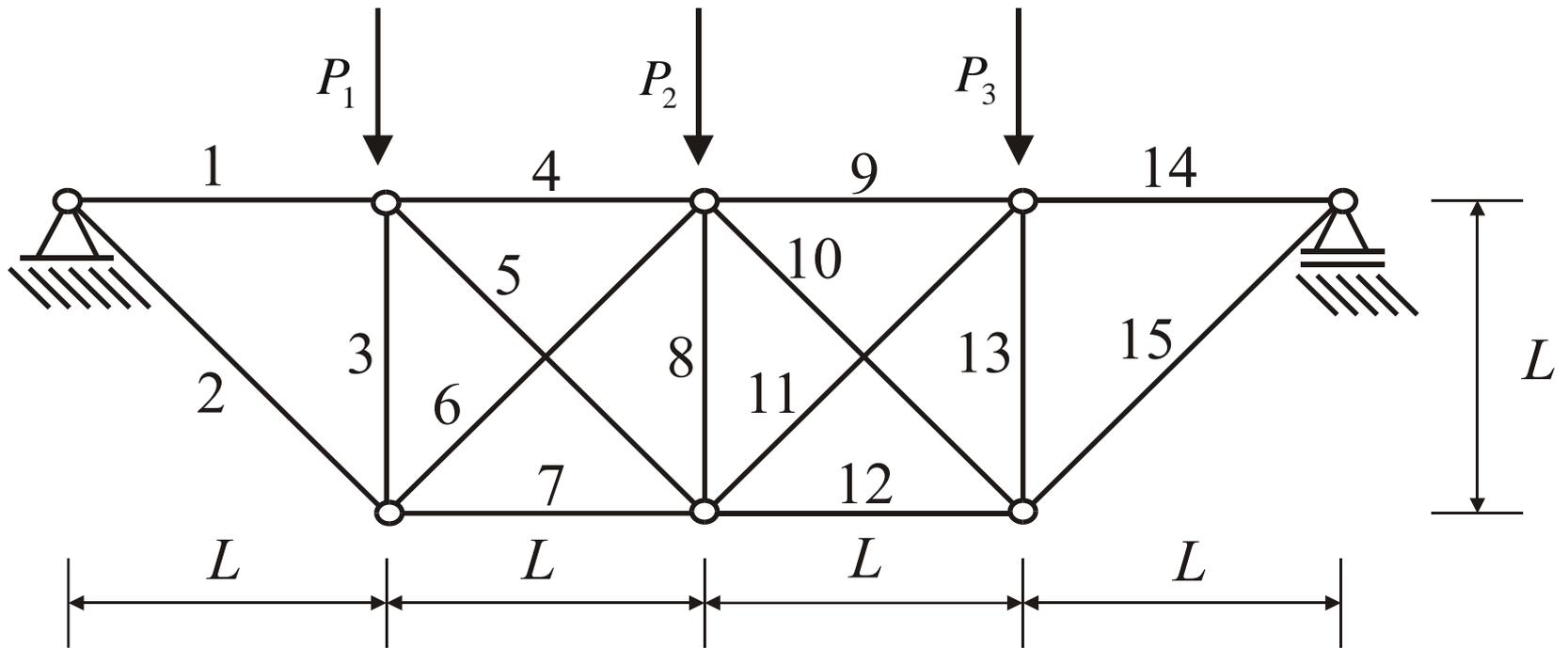


Modeling of Uncertainty in Computational Mechanics

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Truss structure

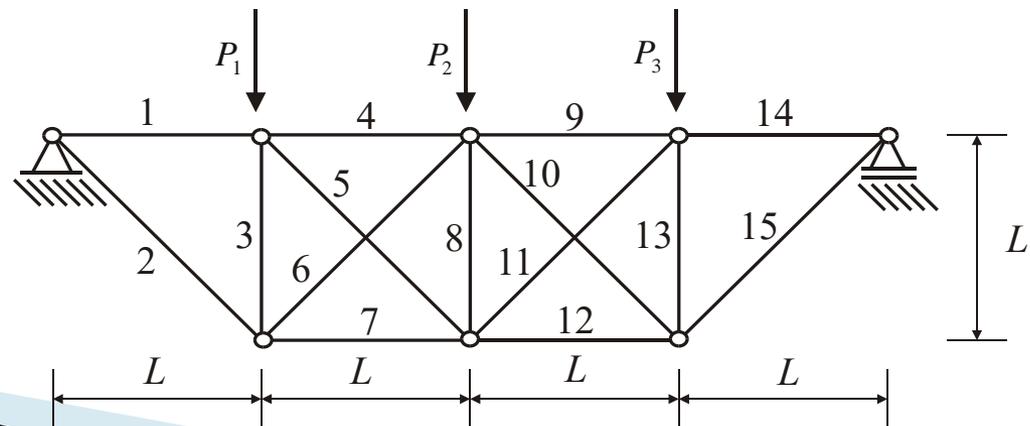


Perturbated forces

$$P = P_0 \pm \Delta P$$

5% uncertainty

No	1	2	3	4	5	6	7	8
ERROR %	10	9,998586	10,00184	10,00126	60,18381	11,67825	9,998955	31,8762
No	9	10	11	12	13	14	15	
ERROR %	10,00126	11,67825	60,18381	9,998955	10,00184	10	9,998586	



Interval equations

$$ax = b \qquad x = \frac{b}{a}$$

Example

$$[1, 2]x = [1, 4]$$

$$x = ?$$

Interval FEM

- ▶ http://en.wikipedia.org/wiki/Interval_finite_element

Differences between intervals and uniformly distributed random variables

Interval



Random variable



Differences between intervals and uniformly distributed random variables

Intervals

$$\mathbf{p}_1 + \dots + \mathbf{p}_m = \left[\sum_i \underline{p}_i, \sum_i \bar{p}_i \right] = n \left[\underline{p}, \bar{p} \right]$$

$$\text{width}(n\mathbf{p}) = n(\bar{p} - \underline{p}) = n \cdot \text{width}(\mathbf{p})$$

Random variables

$$\sigma_{n\mathbf{p}} = \sqrt{\sum_i \sigma_i^2} = \sqrt{n\sigma^2} = \sigma\sqrt{n}$$

$$\text{width}(n\mathbf{p}) = \sqrt{n} \cdot \text{width}(\mathbf{p})$$

Differences between intervals and uniformly distributed random variables

$$\frac{\text{width}(n\mathbf{p}_{\text{int}})}{\text{width}(n\mathbf{p}_{\text{rand}})} = \frac{n \cdot \text{width}(\mathbf{p}_{\text{int}})}{\sqrt{n} \cdot \text{width}(\mathbf{p}_{\text{rand}})} = \sqrt{n}$$

Example $n=100$

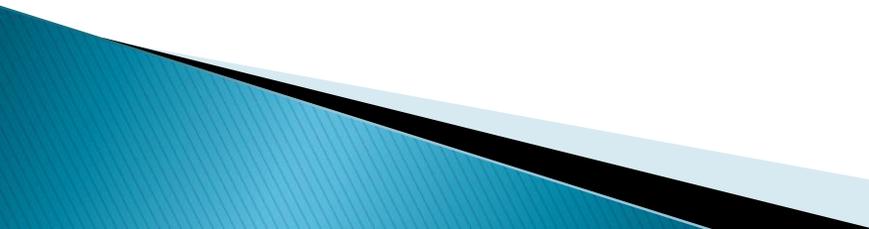
$$\frac{\text{width}(n\mathbf{p}_{\text{int}})}{\text{width}(n\mathbf{p}_{\text{rand}})} = \frac{n \cdot \text{width}(\mathbf{p}_{\text{int}})}{\sqrt{n} \cdot \text{width}(\mathbf{p}_{\text{rand}})} = \sqrt{100} = 10$$

Partial safety factors for materials

$$S_d = \frac{S_u}{\gamma_m}$$

- ▶ S_d – design value
- ▶ S_c – characteristic value

Partial safety factor for materials, account for

- ▶ (i) the possibility of unfavourable deviation of material strength from the characteristic value.
 - ▶ (ii) the possibility of unfavourable variation of member sizes.
 - ▶ (iii) the possibility of unfavourable reduction in member strength due to fabrication and tolerances.
 - ▶ (iv) uncertainty in the calculation of strength of the members.
- 

Partial safety factors for loads

$$F_d = \gamma_f F_c$$

- ▶ F_d – design value
- ▶ F_c – characteristic value

Limit state is a function of safety factors

$$\varphi R > \alpha D + \psi \gamma (\alpha_L L + \alpha_Q Q + \alpha_T T)$$

$$\varphi R - (\alpha D + \psi \gamma (\alpha_L L + \alpha_Q Q + \alpha_T T)) > 0$$

$$L(\gamma_i, \theta) > 0 \Rightarrow \theta$$

Calibration of safety factors

$$L(\gamma_{i\alpha}) > 0$$



$$P_f < P_{f0}$$

$\alpha = P_f$ – probability of failure

Probability of failure

- ▶ Probability of failure =
- ▶ = (number of safe cases)/(number of all cases)

$$P_f = \int_{g(x) < 0} f_X(x) dx$$

structure fail often
=
structure is not safe

Probabilistic vs nonprobabilistic methods

- ▶ Probabilistic methods
 - How often the structure fail?
- ▶ Non-probabilistic methods (worst case design)
 - How big force the structure is able to survive?

Probabilistic design

$$P_f(\theta) = P\{g(x, \theta) < 0\} = \int_{g(x, \theta) < 0} f(x, \theta) dx$$

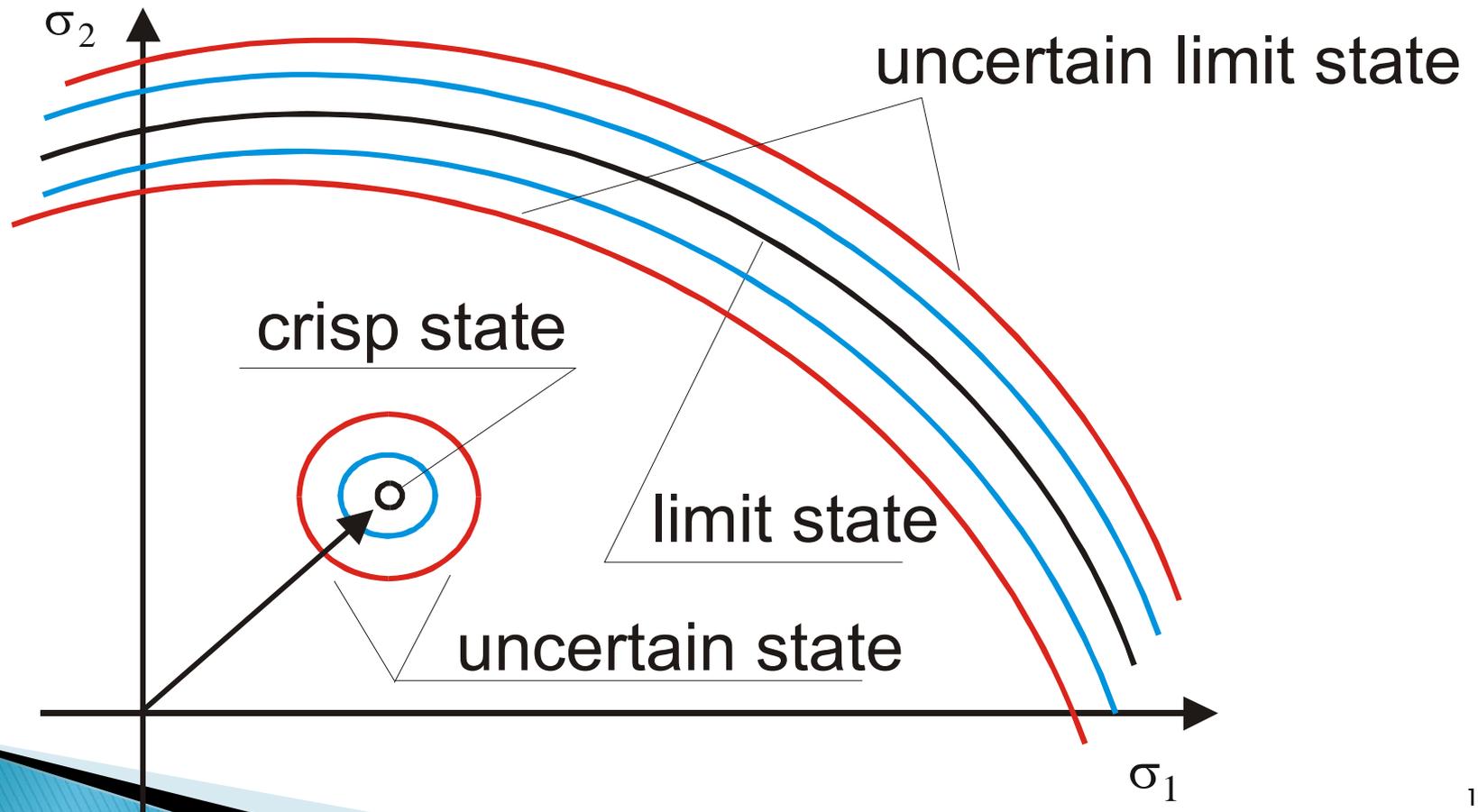
$$P_f(\theta) \leq P_{f_0} \Rightarrow \theta$$

- ▶ Elishakoff I., 2000, Possible limitations of probabilistic methods in engineering. Applied Mechanics Reviews, Vol.53, No.2,pp.19–25

- ▶ Does God play dice?



More complicated safety conditions



Uncertain parameters

Set valued random variable

$$h : \Omega \ni \omega \rightarrow h(\omega) \subseteq R^n$$

Upper and lower probability

$$Pl(A) = P\{\omega : h(\omega) \cap A \neq \emptyset\}$$

$$Bel(A) = P\{\omega : h(\omega) \subseteq A\}$$

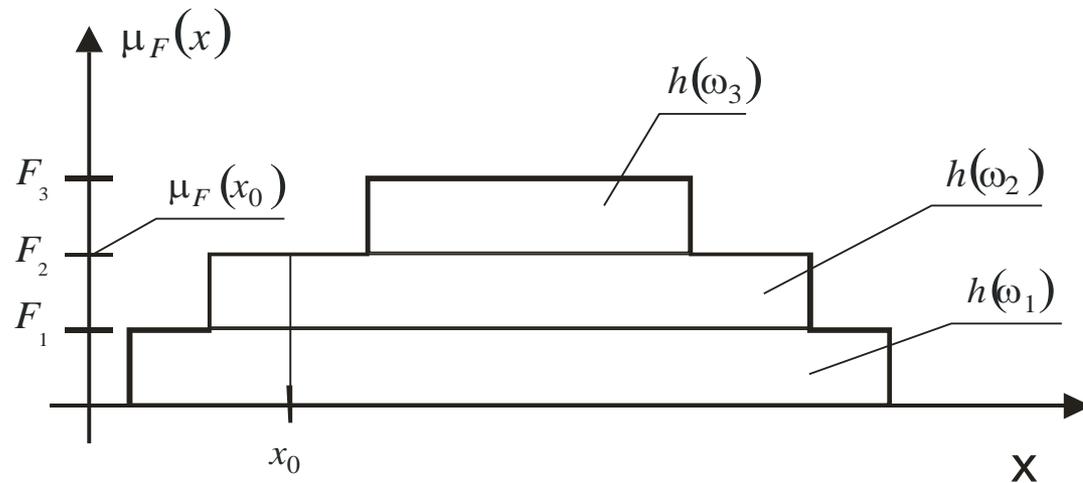
Design under uncertainty

$$Pl(\theta) \leq P_0 \Rightarrow \theta$$

Uncertain parameters

- ▶ Nested family of random sets

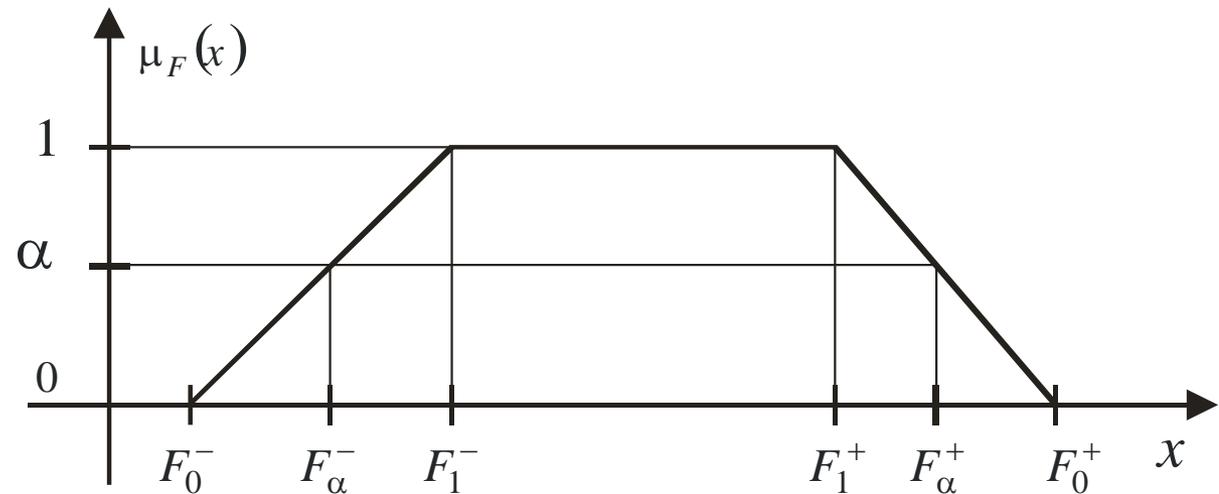
$$h(\omega_1) \supseteq h(\omega_2) \supseteq \dots \supseteq h(\omega_N)$$



$$\mu_F(x) = P\{\omega : x \in h(\omega)\}$$

Uncertain parameters

- ▶ Fuzzy sets



Extension principle

$$\mu_{f(F)}(y) = \sup_{x: y=f(x)} \mu_F(x)$$

Design with fuzzy parameters

$$g(x_F, \theta) \geq 0$$

$$\theta_\alpha = \{ \theta : g(x, \theta) \geq 0, x \in x_\alpha \}$$

$$\mu_\theta(\theta) = \max \{ \alpha : \theta \in \theta_\alpha \}$$

Fuzzy sets and probability

- ▶ <http://andrzej.pownuk.com/fuzzy.htm>
- ▶ Fuzzy approach (the use of grades) is similar to the concept of safety factor.

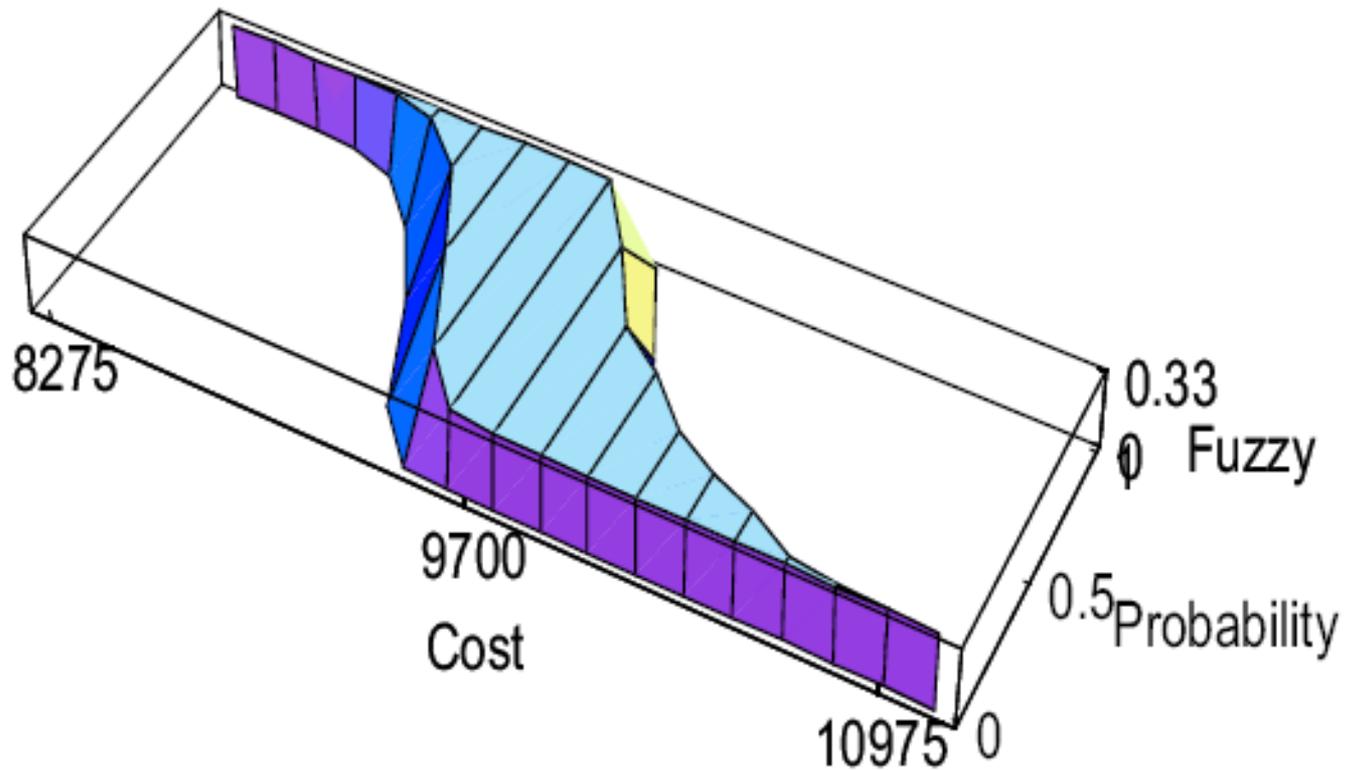
Because of that fuzzy approach is very important.

Alpha cut method

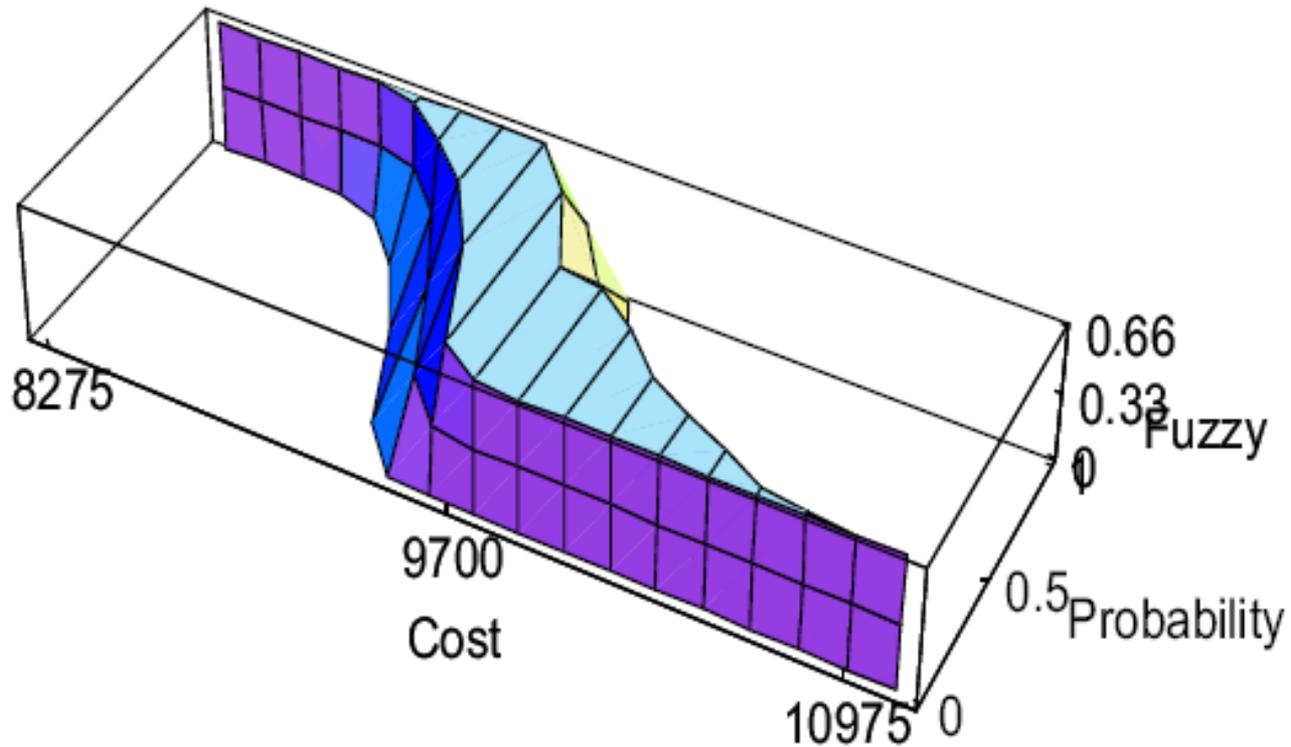
$$\mu_F(x) = \max \left\{ \alpha : x \in [F_\alpha, \bar{F}_\alpha] \right\}$$

$$\mu_R(c, p) = \max \left\{ \alpha : (p, c) \in R_\alpha \right\}$$

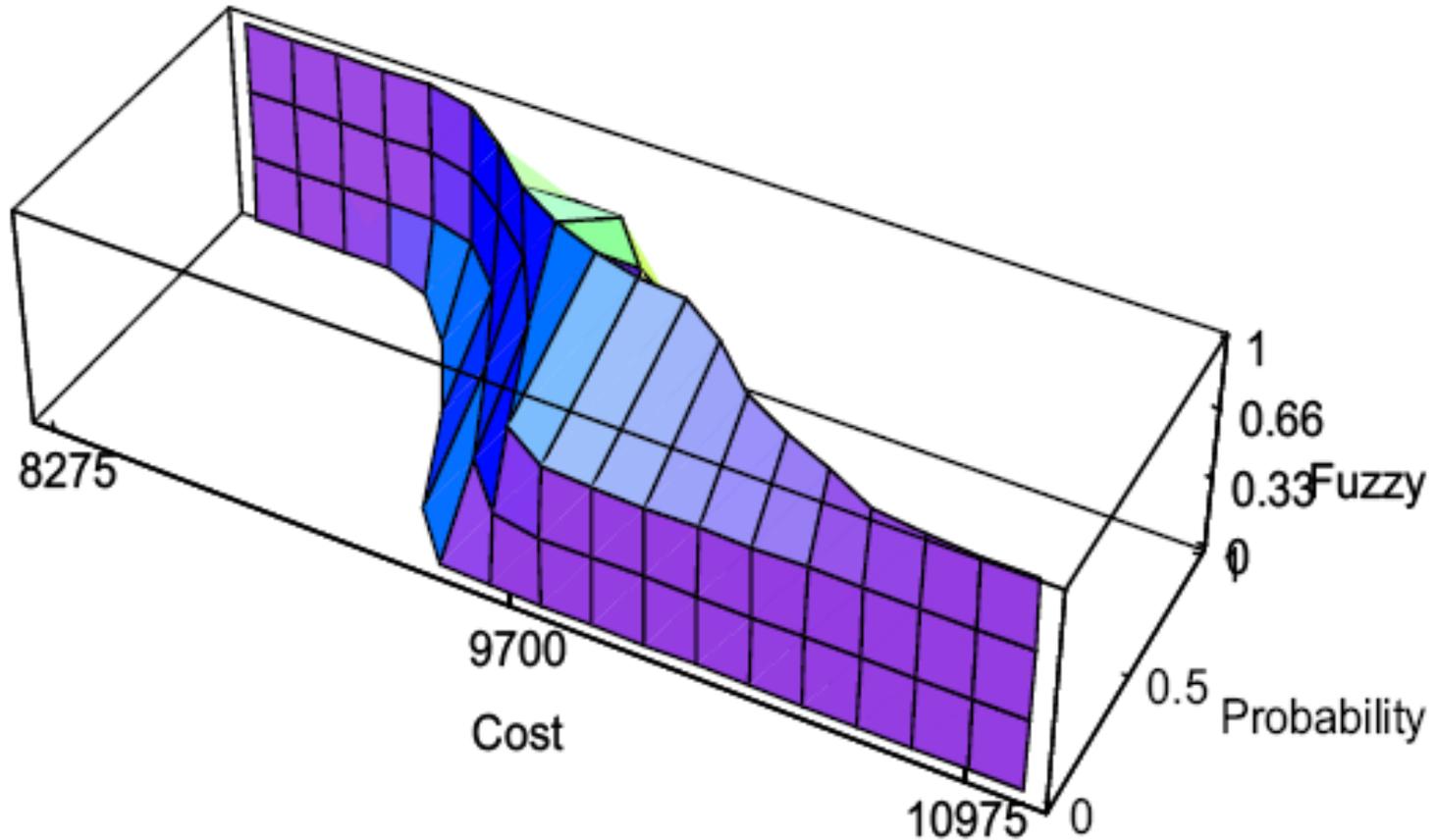
Interval risk curve for different



Interval risk curve for different uncertainty



Interval risk curve for different



Bayesian inference (subjective probability)

$$P(H | E) = \frac{P(E | H)P(H)}{P(E)}$$

$P(H)$ – is called the *prior probability* of H that was inferred before new evidence, E , became available

$P(E | H)$ – is called the *conditional probability* of seeing the evidence E if the hypothesis H happens to be true.
It is also called a *likelihood function* when it is considered as a function of H for fixed E .

$P(E)$ – marginal probability

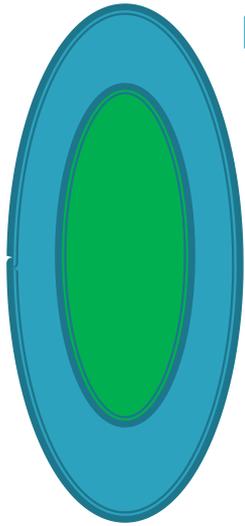
$P(H | E)$ – is called the *posterior probability* of H given E .

Cox's theorem

- ▶ **Cox's theorem**, named after the physicist Richard Threlkeld Cox, is a derivation of the laws of probability theory from a certain set of postulates. This derivation justifies the so-called "logical" interpretation of probability. As the laws of probability derived by Cox's theorem are applicable to any proposition, logical probability is a type of Bayesian probability. Other forms of Bayesianism, such as the subjective interpretation, are given other justifications.

Rough sets, soft sets

(sets with features)



- ▶ First described by Zdzisław I. Pawlak, is a formal approximation of a crisp set (i.e., conventional set) in terms of a pair of sets which give the *lower* and the *upper* approximation of the original set. In the standard version of rough set theory (Pawlak 1991), the lower- and upper-approximation sets are crisp sets, but in other variations, the approximating sets may be fuzzy sets.

Interval and set valued parameters



Interval parameters

$$p \in [\underline{p}, \bar{p}]$$

Design with the interval parameters

$$g(p, \theta) \geq 0$$

$$\boldsymbol{\theta} = \{ \theta : g(p, \theta) \geq 0, p \in \mathbf{p} \}$$

Important papers

- ▶ R. E. Moore. Interval Analysis. Prentice–Hall, Englewood Cliffs N. J., 1966
- ▶ Neumaier A., 1990, Interval methods for systems of equations, Cambridge University Press, New York
- ▶ Ben–Haim Y., Elishakoff I., 1990, Convex Models of Uncertainty in Applied Mechanics. Elsevier Science Publishers, New York
- ▶ Buckley J.J., Qy Y., 1990, On using α -cuts to evaluate fuzzy equations. Fuzzy Sets and Systems, Vol.38,pp.309–312

Important papers

- ▶ Köylüoğlu H.U., A.S. Çakmak, and S. R. K. Nielsen (1995). “Interval Algebra to Deal with Pattern Loading of Structural Uncertainties,” *ASCE Journal of Engineering Mechanics*, 11, 1149–1157

Important papers

- ▶ Rump S.M., 1994, Verification methods for dense and sparse systems of equations. J. Herzberger, ed., Topics in Validated Computations. Elsevier Science B.V., pp.63–135

Important papers

- ▶ Muhanna in the paper Muhanna R.L., Mullen R.L., Uncertainty in Mechanics Problems – Interval – Based Approach. Journal of Engineering Mechanics, Vol.127, No.6, 2001, 557–556
- ▶ E.Popova, On the Solution of Parametrised Linear Systems. W. Kraemer, J. Wolff von Gudenberg (Eds.): Scientific Computing, Validated Numerics, Interval Methods. Kluwer Acad. Publishers, 2001, pp. 127–138.

Important papers

- ▶ I. Skalna, A Method for Outer Interval Solution of Systems of Linear Equations Depending Linearly on Interval Parameters, Reliable Computing, Volume 12, Number 2, April, 2006, Pages 107–120

Important papers

- ▶ Akpan U.O., Koko T.S., Orisamolu I.R., Gallant B.K., Practical fuzzy finite element analysis of structures, Finite Elements in Analysis and Design, 38 (2000) 93–111
- ▶ McWilliam, Stewart, 2001
Anti-optimisation of uncertain structures using interval analysis
Computers and Structures Volume: 79, Issue: 4, February, 2001, pp. 421–430

Important papers

- ▶ Pownuk A., Numerical solutions of fuzzy partial differential equation and its application in computational mechanics, Fuzzy Partial Differential Equations and Relational Equations: Reservoir Characterization and Modeling (M. Nikraves, L. Zadeh and V. Korotkikh, eds.), Studies in Fuzziness and Soft Computing, Physica-Verlag, 2004, pp.308–347

Important papers

- ▶ Neumaier A., Clouds, fuzzy sets and probability intervals, Reliable Computing 10: 249–272, 2004
- ▶ <http://andrzej.pownuk.com/IntervalEquations.htm>

Examples

- ▶ <http://webapp.math.utep.edu:8080/~andrzej/php/ansys2interval/>
- ▶ <http://webapp.math.utep.edu/Pages/IntervalFEMExamples.htm>
- ▶ <http://calculus.math.utep.edu/IntervalODE-1.0/default.aspx>
- ▶ <http://calculus.math.utep.edu/AdaptiveTaylorSeries-1.1/default.aspx>
- ▶ <http://andrzej.pownuk.com/silverlight/VibrationsWithIntervalParameters/VibrationsWithIntervalParameters.html>

Interval equations

$$ax = b \qquad x = \frac{b}{a}$$

Example

$$[1, 2]x = [1, 4]$$

$$x = ?$$

Algebraic solution

$$[1, 2]x = [1, 4]$$

$$x = [1, 2]$$

because

$$[1, 2][1, 2] = [1, 4]$$

Algebraic solution

$$[1, 4]x = [1, 4]$$

$$x = [1, 1] = 1$$

because

$$[1, 4] \cdot 1 = [1, 4]$$

Algebraic solution

$$[1, 8]x = [1, 4]$$

$$x = ?$$

United solution set

$$[1, 2]x = [1, 4]$$

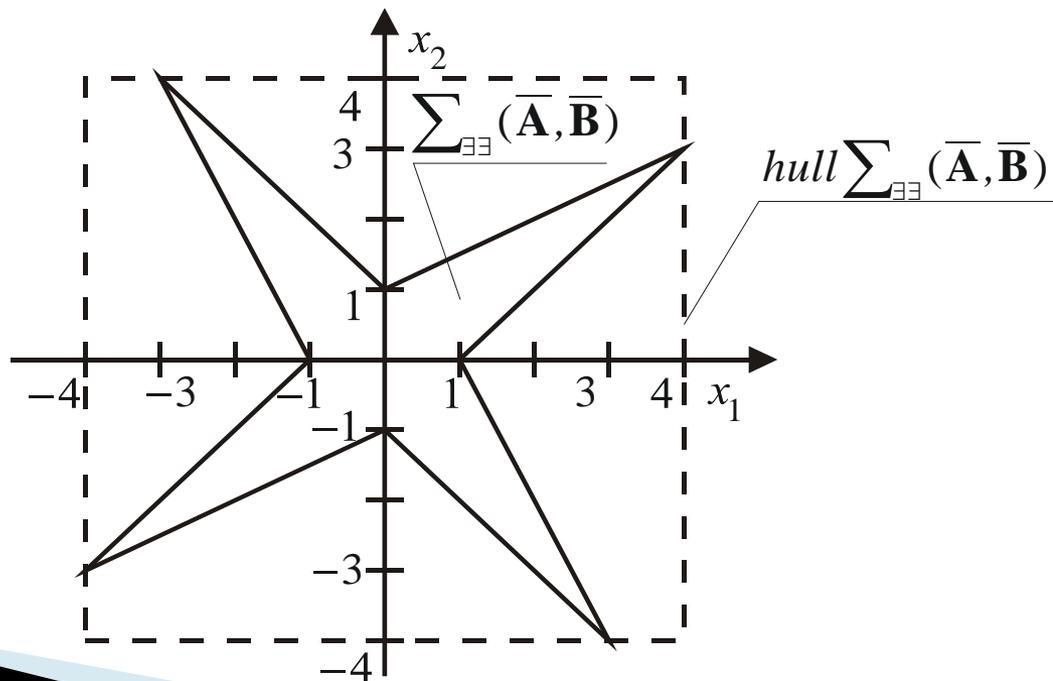
$$\mathbf{x} = \left[\frac{1}{2}, 4 \right]$$

because

$$\mathbf{x} = \{x : ax = b, a \in [1, 2], b \in [1, 4]\}$$

United solution set

$$\begin{bmatrix} [1,2] & [2,4] \\ [2,4] & [1,2] \end{bmatrix} \cdot \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} [-1,1] \\ [1,2] \end{bmatrix}$$



Different solution sets

United solution set

$$\sum_{\exists\exists}(\mathbf{A}, \mathbf{b}) = \{x : \exists A \in \mathbf{A}, \exists b \in \mathbf{b}, Ax = b\}$$

Tolerable solution set

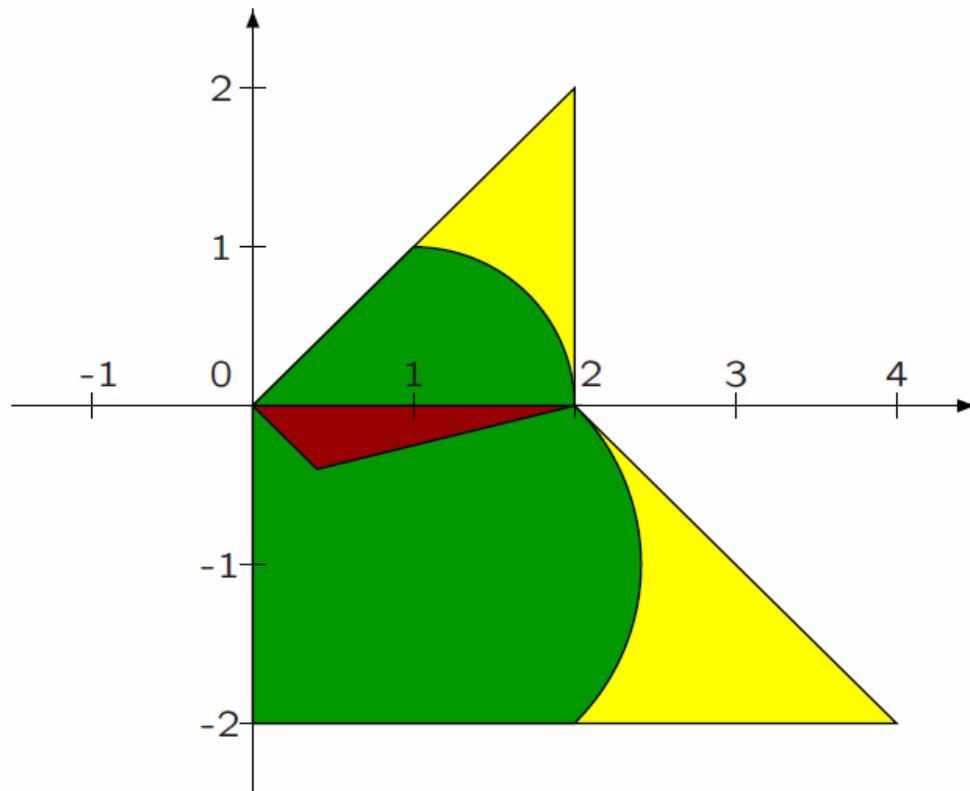
$$\sum_{\forall\exists}(\mathbf{A}, \mathbf{b}) = \{x : \forall A \in \mathbf{A}, \exists b \in \mathbf{b}, Ax = b\}$$

Controllable solution set

$$\sum_{\exists\forall}(\mathbf{A}, \mathbf{b}) = \{x : \exists A \in \mathbf{A}, \forall b \in \mathbf{b}, Ax = b\}$$

Other solution sets

$$A = \begin{pmatrix} 1 & [0, 1] \\ [0, 1] & [-4, -1] \end{pmatrix}, \quad b = \begin{pmatrix} [0, 2] \\ [0, 2] \end{pmatrix},$$



■ — Ξ_{uni}

■ — Ξ_{uni}^{sym}

■ — $\Xi_{tol} \equiv \Xi_{tol}^{sym}$

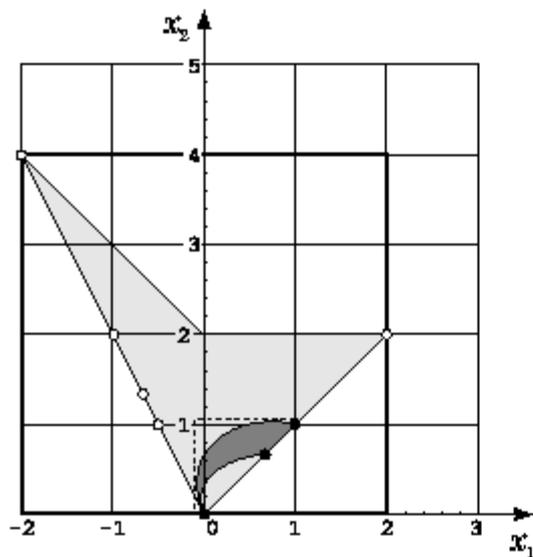
Parametric solution sets

Thus, the *Parametric Solution Set* (PSS) is defined as:

$$\Sigma(\mathbf{A}(\mathbf{p}), \mathbf{b}(\mathbf{p})) = \{ \tilde{\mathbf{x}} \in \mathbb{R}^n \mid (\exists \tilde{\mathbf{p}} \in \mathbf{p}) \mathbf{A}(\tilde{\mathbf{p}}) \tilde{\mathbf{x}} = \mathbf{b}(\tilde{\mathbf{p}}) \}.$$

Contrary to the normal case, *Parametric Boundary Solution Set* does not in general contain extremal points of PSS, so at most:

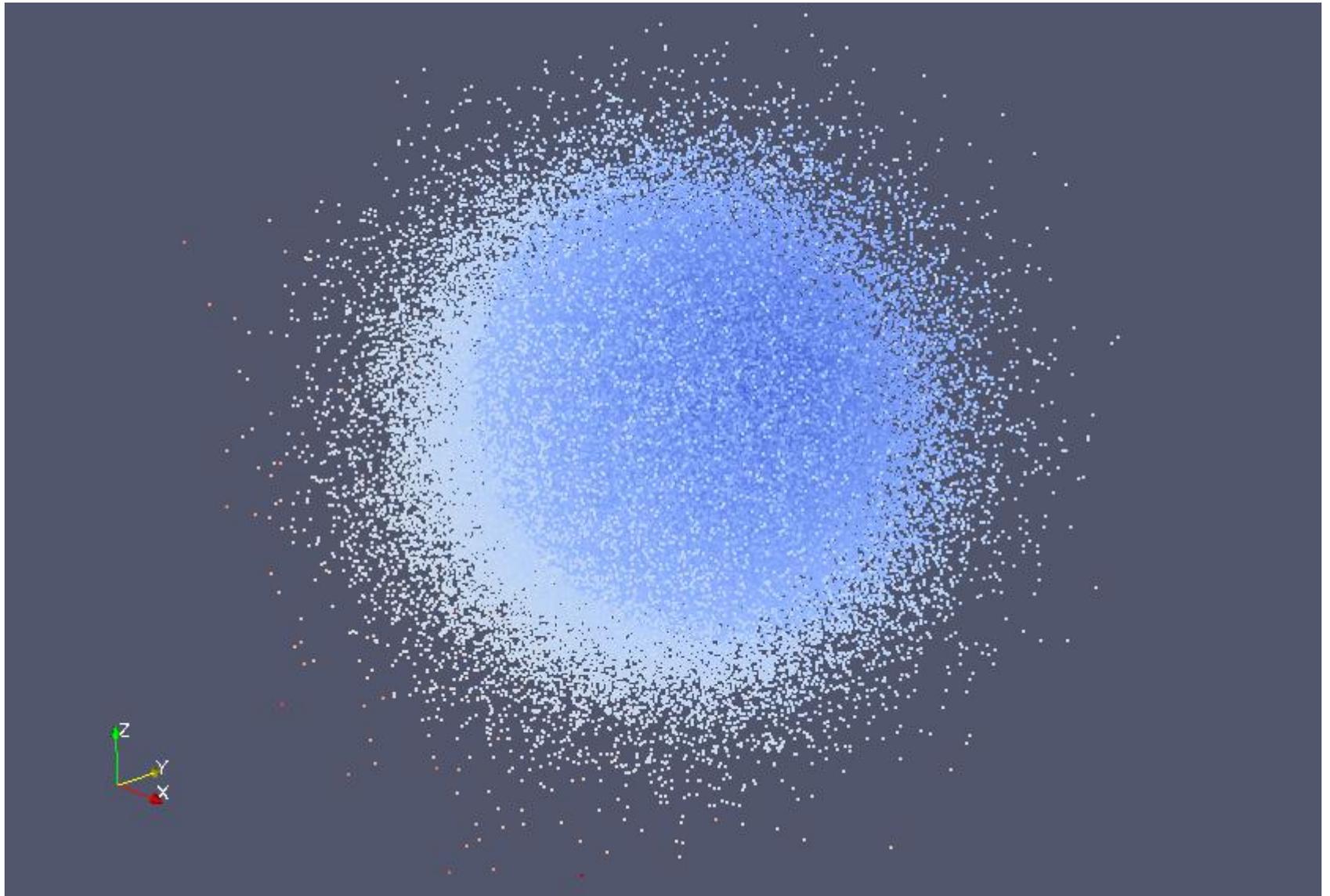
$$\text{hull } \Sigma(\mathbf{A}(\partial\mathbf{p}), \mathbf{b}(\partial\mathbf{p})) \subseteq \text{hull } \Sigma(\mathbf{A}(\mathbf{p}), \mathbf{b}(\mathbf{p})).$$

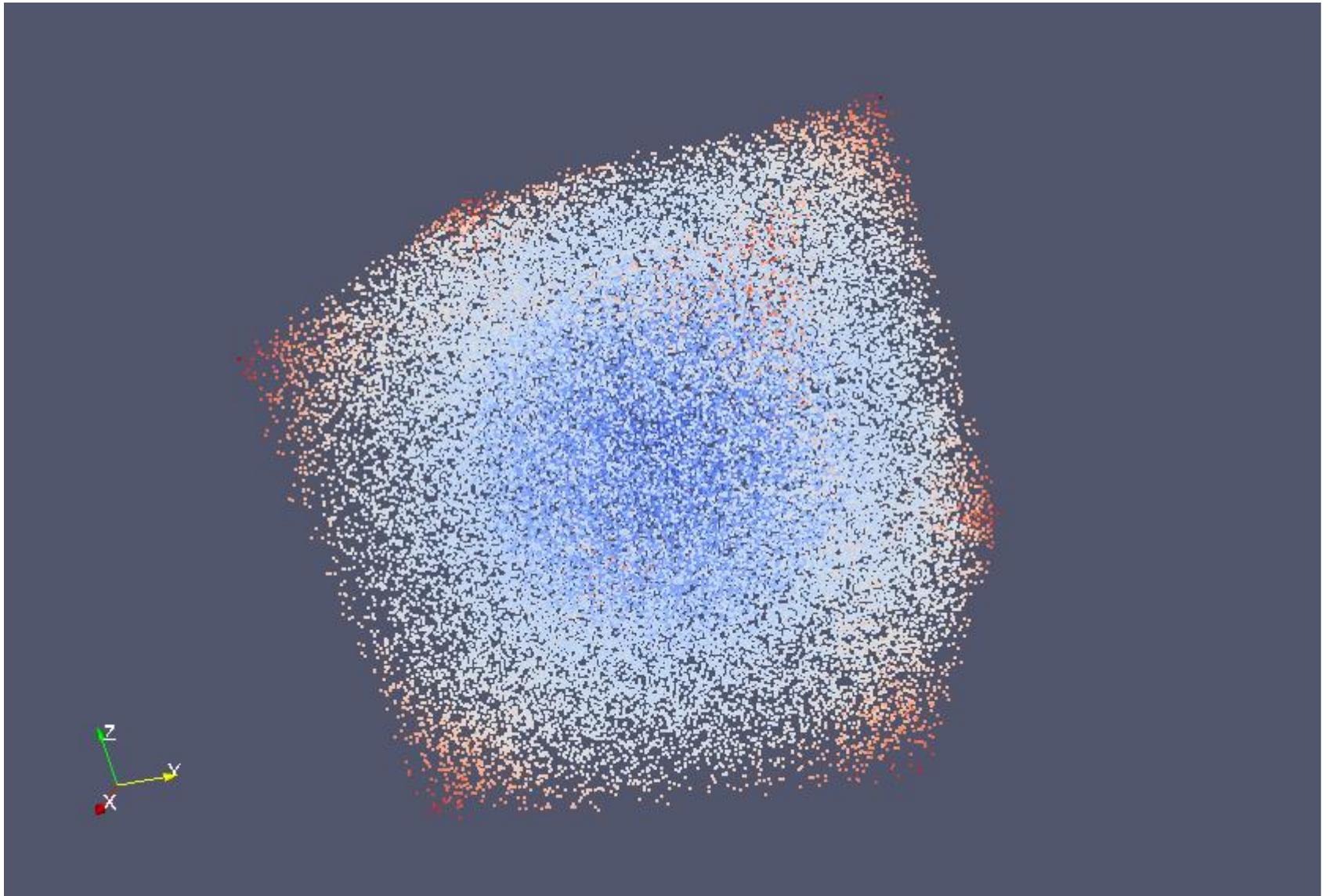


- | | |
|--|--|
| \square $\Sigma(\mathbf{A}, \mathbf{b})$ | ∇ $\Sigma(\mathbf{A}(\mathbf{p}), \mathbf{b}(\mathbf{p}))$ |
| \circ $\Sigma(\partial\mathbf{A}, \partial\mathbf{b})$ | \bullet $\Sigma(\mathbf{A}(\partial\mathbf{p}), \mathbf{b}(\partial\mathbf{p}))$ |
| \square $\text{hull } \Sigma(\mathbf{A}, \mathbf{b})$ | \square $\text{hull } \Sigma(\mathbf{A}(\mathbf{p}), \mathbf{b}(\mathbf{p}))$ |

$$\mathbf{A} = \begin{bmatrix} [0, 1] & [1, 2] \\ -2 & [-1, 2] \end{bmatrix} \quad \mathbf{b} = \begin{bmatrix} [0, 2] \\ 0 \end{bmatrix},$$

$$\mathbf{A}(\mathbf{p}) = \begin{bmatrix} p_1 & 1+p_2 \\ -2 & 3p_1-1 \end{bmatrix} \quad \mathbf{b}(\mathbf{p}) = \begin{bmatrix} 2p_1 \\ 0 \end{bmatrix}, \quad p_1, p_2 \in [0, 1]$$





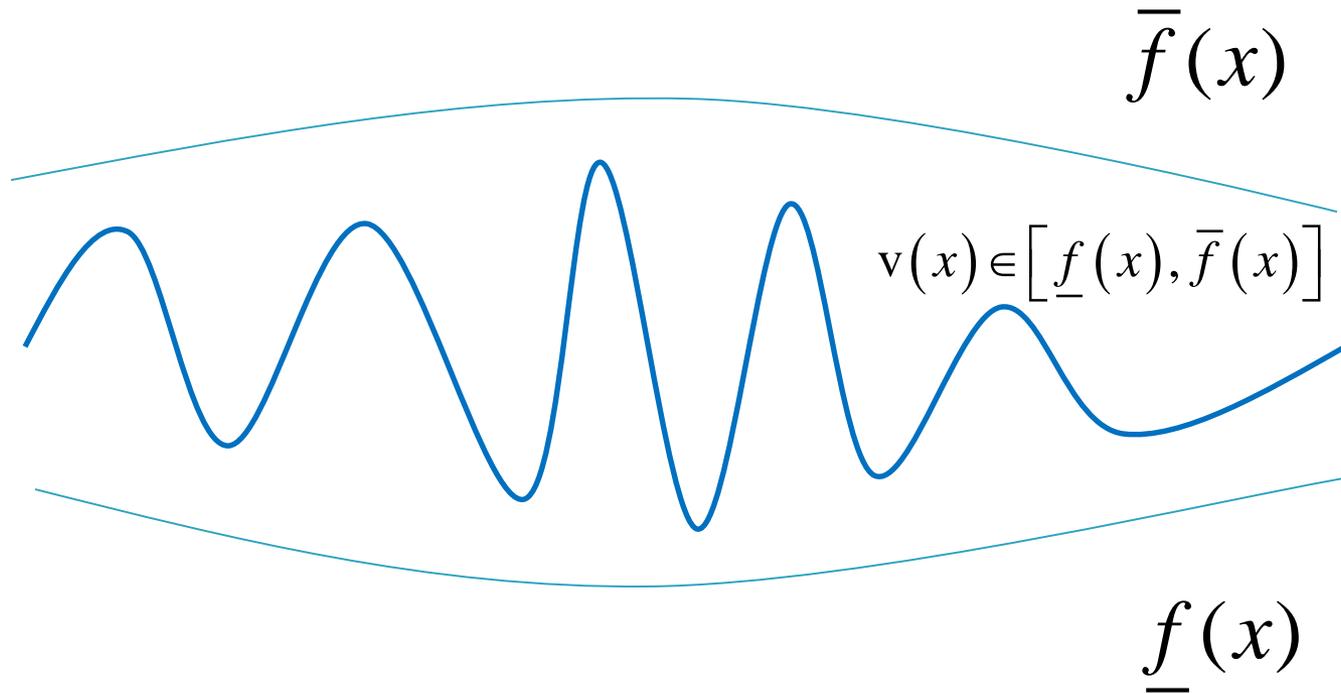
Derivative

$$f(x) = \left[\underline{f}(x), \bar{f}(x) \right]$$

$$f'(x) = \left[\min \{ \underline{f}'(x), \bar{f}'(x) \}, \max \{ \underline{f}'(x), \bar{f}'(x) \} \right]$$

What is the definition of the solution of differential equation?

Differentiation of the interval function

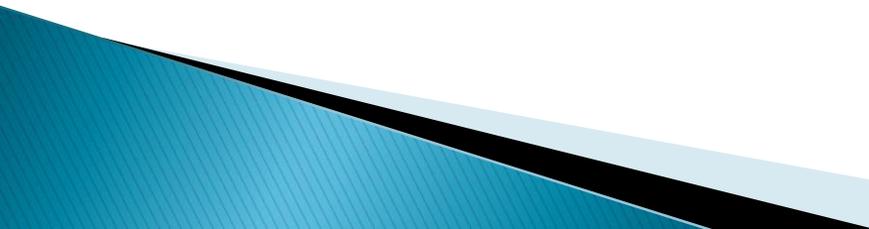


$$v'(x) \notin \left[\min \{ \underline{f}'(x), \bar{f}'(x) \}, \max \{ \underline{f}'(x), \bar{f}'(x) \} \right]$$

What is the definition of the solution of differential equation?

Dubois D., Prade H., 1987, On Several Definition of the Differentiation of Fuzzy Mapping,
Fuzzy Sets and Systems, Vol.24, pp.117–120

How about integral equations?



Other problems

- ▶ Modal interval arithmetic
- ▶ Affine arithmetic
- ▶ Constrain interval arithmetic
- ▶ Ellipsoidal arithmetic
- ▶ Convex models (equations with the ellipsoidal parameters)
- ▶ General set valued arithmetic
- ▶ Fuzzy relational equations
- ▶ Etc.

Methods of solutions



What does
everyone
have in mind?



Taylor expansion

$$y(p_1, \dots, p_m) \approx y(p_{10}, \dots, p_{m0}) + \frac{\partial y}{\partial p_1} (p_1 - p_{10}) + \dots + \frac{\partial y}{\partial p_m} (p_m - p_{m0})$$

$$y_0 = y(p_{10}, \dots, p_{m0})$$

$$\Delta y \approx \left| \frac{\partial y}{\partial p_1} \right| \Delta p_1 + \dots + \left| \frac{\partial y}{\partial p_m} \right| \Delta p_m$$

$$y \in [\underline{y}, \bar{y}] \approx [y_0 - \Delta y, y_0 + \Delta y]$$

General optimization methods

- ▶ Gradient descent
 - ▶ Interior point method
 - ▶ Sequential quadratic programming
 - ▶ Genetic algorithms
 - ▶ ...
- 

Interval methods and reliable computing



System of linear interval equations

- ▶ Endpoint combination method
 - ▶ Interval Gauss elimination
 - ▶ Interval Gauss–Seidel method
 - ▶ Linear programming method
 - ▶ Rohn method
-
- ▶ Jiri Rohn, "A Handbook of Results on Interval Linear Problems", 2006
<http://www.cs.cas.cz/~rohn/publist/handbook.zip>

Oettli and Prager (1964)

$$x \in \sum_{\exists \exists} (\mathbf{A}, \mathbf{b}) \Leftrightarrow |mid(\mathbf{A})x - rad(\mathbf{b})| \leq (rad(\mathbf{A})x + rad(\mathbf{b}))$$

$$A \in \mathbf{A}, b \in \mathbf{b}$$

- ▶ W. Oettli, W. Prager. Compatibility of approximate solution of linear equations with given error bounds for coefficients and right-hand sides. Numer. Math. 6: 405–409, 1964.

Linear programming method

$$\left\{ \begin{array}{l} \min x_i \\ (mid(\mathbf{A})D_s - rad(\mathbf{A}))x \leq \bar{b} \\ (mid(\mathbf{A})D_s + rad(\mathbf{A}))x \geq \bar{b} \\ x \geq 0 \end{array} \right. \quad \left\{ \begin{array}{l} \max x_i \\ (mid(\mathbf{A})D_s - rad(\mathbf{A}))x \leq \bar{b} \\ (mid(\mathbf{A})D_s + rad(\mathbf{A}))x \geq \bar{b} \\ x \geq 0 \end{array} \right.$$

- ▶ H.U. Koyluoglu, A. Çakmak, S.R.K. Nielsen. Interval mapping in structural mechanics. In: Spanos, ed. Computational Stochastic Mechanics. 125–133. Balkema, Rotterdam 1995.

Rohn's method

$$\begin{cases} A_{rc} = \text{mid}(\mathbf{A}) - D_r(\text{rad}\mathbf{A})D_c \\ b_r = \text{mid}(\mathbf{b}) + D_r \text{rad}(\mathbf{b}) \end{cases}$$

$$r = (1, -1, 1, \dots, 1)^T \in J$$

$$\text{conv} \sum_{\exists \exists} (\mathbf{A}, \mathbf{b}) = \text{conv} \sum_{\exists \exists} (\mathbf{A}_{rc}, \mathbf{b}_{rc})$$

$$\text{conv} \sum_{\exists \exists} (\mathbf{A}_{rc}, \mathbf{b}_{rc}) = \text{conv} \{x : A_{rc}x = b_r, r, c \in J\}$$

Rohn's method $2^n \cdot 2^n = 2^{2n}$

Combinatoric solution 2^{n^2+n}

Rohn sign–accord method (RSA)

- ▶ For every $r \in J$
- ▶ Select $c \in J$ recommended $c = \text{sign}\left(\text{mid}(\mathbf{A})^{-1} b_r\right)$
- ▶ Solve $A_{rc}x = b_r$
- ▶ If $\text{sign}(x) = c$ then register x and go to next r
- ▶ Otherwise find $k = \min\{j : \text{sign}(x_j) \neq c_j\}$
- ▶ Set $c_k = -c_k$ and go to step 1.

Software

VERSOFT: Verification software in MATLAB / INTLAB

<http://uivtx.cs.cas.cz/~rohn/matlab/index.html>

- Real data only: Linear systems (rectangular)
- Verified description of all solutions of a system of linear equations
- Verified description of all linear squares solutions of a system of linear equations
- Verified nonnegative solution of a system of linear inequalities
- VERLINPROG for verified nonnegative solution of a system of linear equations
- Real data only: Matrix equations (rectangular)
- See VERMATREQN for verified solution of the matrix equation $A*X*B+C*X*D=F$ (in particular, of the Sylvester or Lyapunov equation)

Etc.

Muhanna and Mullen

Fixed point theory

- ▶ Find the solution of $Ax = b$
 - Transform into fixed point equation $g(x) = x$
 $g(x) = x - R(Ax - b) = Rb + (I - RA)x$ (R nonsingular)
 - Brouwer's fixed point theorem
*If $Rb + (I - RA)X \subseteq \text{int}(X)$
then $\exists x \in X, Ax = b$*

Fixed point theory

▶ Solve $AX=b$

- Brouwer's fixed point theorem w/
Krawczyk's operator

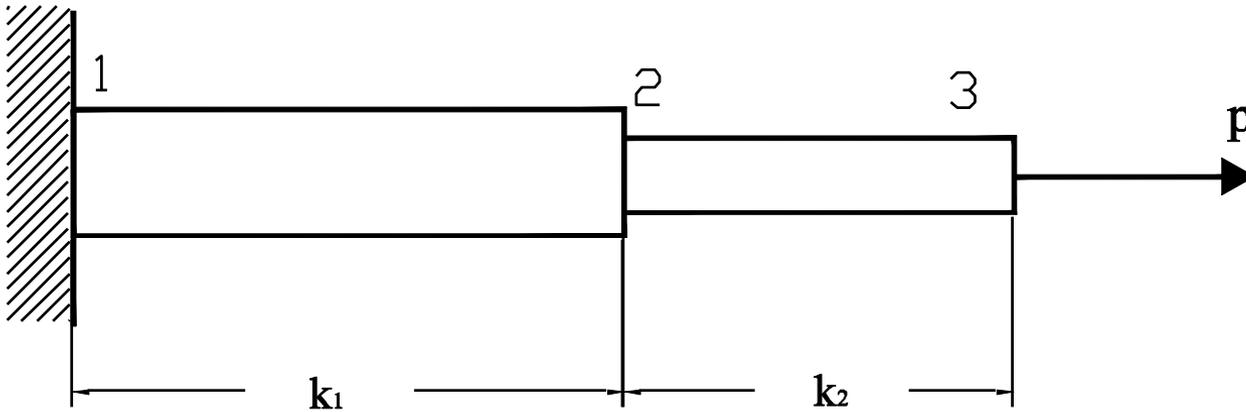
If $Rb + (I - RA)X \subseteq \text{int}(X)$

then $\Sigma(A, b) \subseteq X$

- Iteration

- $X^{n+1} = Rb + (I - RA) \epsilon X^n$ (for $n = 0, 1, 2, \dots$)
- Stopping criteria: $X^{n+1} \subseteq \text{int}(X^n)$
- Enclosure: $\Sigma(A, b) \subseteq X^{n+1}$

Dependency problem



$$\begin{pmatrix} k_1 + k_2 & -k_2 \\ -k_2 & k_2 \end{pmatrix} \begin{pmatrix} u_1 \\ u_2 \end{pmatrix} = \begin{pmatrix} 0 \\ p \end{pmatrix}$$

Dependency problem

$$\mathbf{k}_1 = [0.9, 1.1], \mathbf{k}_2 = [1.8, 2.2], p = 1.0$$

$$\mathbf{u}_1 = \frac{1}{\mathbf{k}_1} = \frac{1}{[0.9, 1.1]} = [0.91, 1.11]$$

$$\mathbf{u}_2 = \frac{\mathbf{k}_1 + \mathbf{k}_2}{\mathbf{k}_1 \mathbf{k}_2} = \frac{[0.9, 1.1] + [1.8, 2.2]}{[0.9, 1.1] \times [1.8, 2.2]} = [1.12, 2.04]$$

(overestimation)

$$\mathbf{u}_2' = \frac{1}{\mathbf{k}_1} + \frac{1}{\mathbf{k}_2} = \frac{1}{[0.9, 1.1]} + \frac{1}{[1.8, 2.2]} = [1.36, 1.67]$$

(exact solution)

Dependency problem

$$\mathbf{u}_2 = \frac{\mathbf{k}_1 + \mathbf{k}_2}{\mathbf{k}_1 \mathbf{k}_2}$$

- ▶ Two \mathbf{k}_1 : the same physical quantity
- ▶ Interval arithmetic: treat two \mathbf{k}_1 as two independent interval quantities having same bounds

Naïve interval finite element

- ▶ Replace floating point arithmetic by interval arithmetic
- ▶ Over-pessimistic result due to dependency

$$\begin{pmatrix} [2.7, 3.3] & [-2.2, -1.8] \\ [-2.2, -1.8] & [1.8, 2.2] \end{pmatrix} \begin{pmatrix} \mathbf{u}_1 \\ \mathbf{u}_2 \end{pmatrix} = \begin{pmatrix} 0 \\ 1 \end{pmatrix}$$

Naïve solution

$$\begin{pmatrix} \mathbf{u}_1 \\ \mathbf{u}_2 \end{pmatrix} = \begin{pmatrix} [-110, 112] \\ [-134.5, 137.5] \end{pmatrix}$$

Exact solution

$$\begin{pmatrix} \mathbf{u}_1 \\ \mathbf{u}_2 \end{pmatrix} = \begin{pmatrix} [0.91, 1.11] \\ [1.36, 1.67] \end{pmatrix}$$

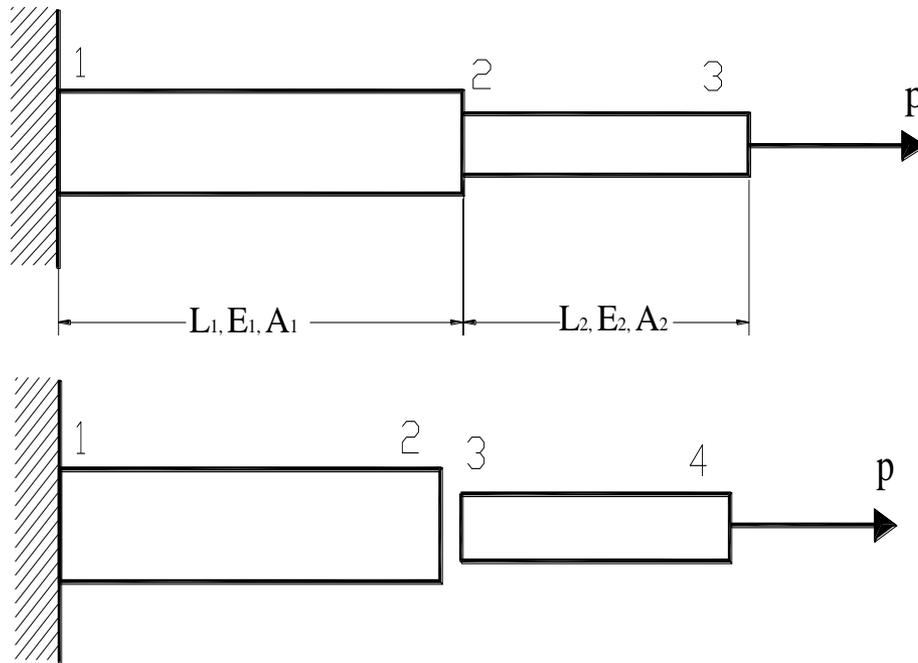
Dependency problem

- ▶ How to reduce overestimation?
 - Manipulate the expression to reduce multiple occurrence
 - Trace the sources of dependency

$$\begin{pmatrix} \mathbf{k}_1 + \mathbf{k}_2 & -\mathbf{k}_2 \\ -\mathbf{k}_2 & \mathbf{k}_2 \end{pmatrix} \begin{pmatrix} \mathbf{u}_1 \\ \mathbf{u}_2 \end{pmatrix} = \begin{pmatrix} \mathbf{0} \\ \mathbf{p} \end{pmatrix}$$

Present formulation

- ▶ Element-by-Element
 - K : diagonal matrix, singular



Present formulation

- ▶ Element-by-element method

- Element stiffness: $\mathbf{K}_i = \check{K}_i(I + \mathbf{d}_i)$

$$\mathbf{K}_1 = \begin{pmatrix} \frac{\mathbf{E}_1 A_1}{L_1} & -\frac{\mathbf{E}_1 A_1}{L_1} \\ -\frac{\mathbf{E}_1 A_1}{L_1} & \frac{\mathbf{E}_1 A_1}{L_1} \end{pmatrix} = \begin{pmatrix} \frac{\check{E}_1 A_1}{L_1} & -\frac{\check{E}_1 A_1}{L_1} \\ -\frac{\check{E}_1 A_1}{L_1} & \frac{\check{E}_1 A_1}{L_1} \end{pmatrix} \left(\begin{pmatrix} 1 & 0 \\ 0 & 1 \end{pmatrix} + \begin{pmatrix} \boldsymbol{\alpha}_1 & 0 \\ 0 & \boldsymbol{\alpha}_1 \end{pmatrix} \right)$$

- System stiffness: $\mathbf{K} = \check{K}(I + \mathbf{d})$

Present formulation

- ▶ Lagrange Multiplier method
 - With the constraints: $CU - t = 0$
 - Lagrange multipliers: λ

$$\begin{pmatrix} K & C^T \\ C & 0 \end{pmatrix} \begin{pmatrix} u \\ \lambda \end{pmatrix} = \begin{pmatrix} p \\ t \end{pmatrix} \Rightarrow \begin{pmatrix} \mathbf{K} & C^T \\ C & 0 \end{pmatrix} \begin{pmatrix} \mathbf{u} \\ \boldsymbol{\lambda} \end{pmatrix} = \begin{pmatrix} \mathbf{p} \\ \mathbf{0} \end{pmatrix}$$

Present formulation

- ▶ System equation: $\mathbf{Ax} = \mathbf{b}$

$$\begin{pmatrix} \mathbf{K} & \mathbf{C}^T \\ \mathbf{C} & \mathbf{0} \end{pmatrix} \begin{pmatrix} \mathbf{u} \\ \boldsymbol{\lambda} \end{pmatrix} = \begin{pmatrix} \mathbf{p} \\ \mathbf{0} \end{pmatrix}$$

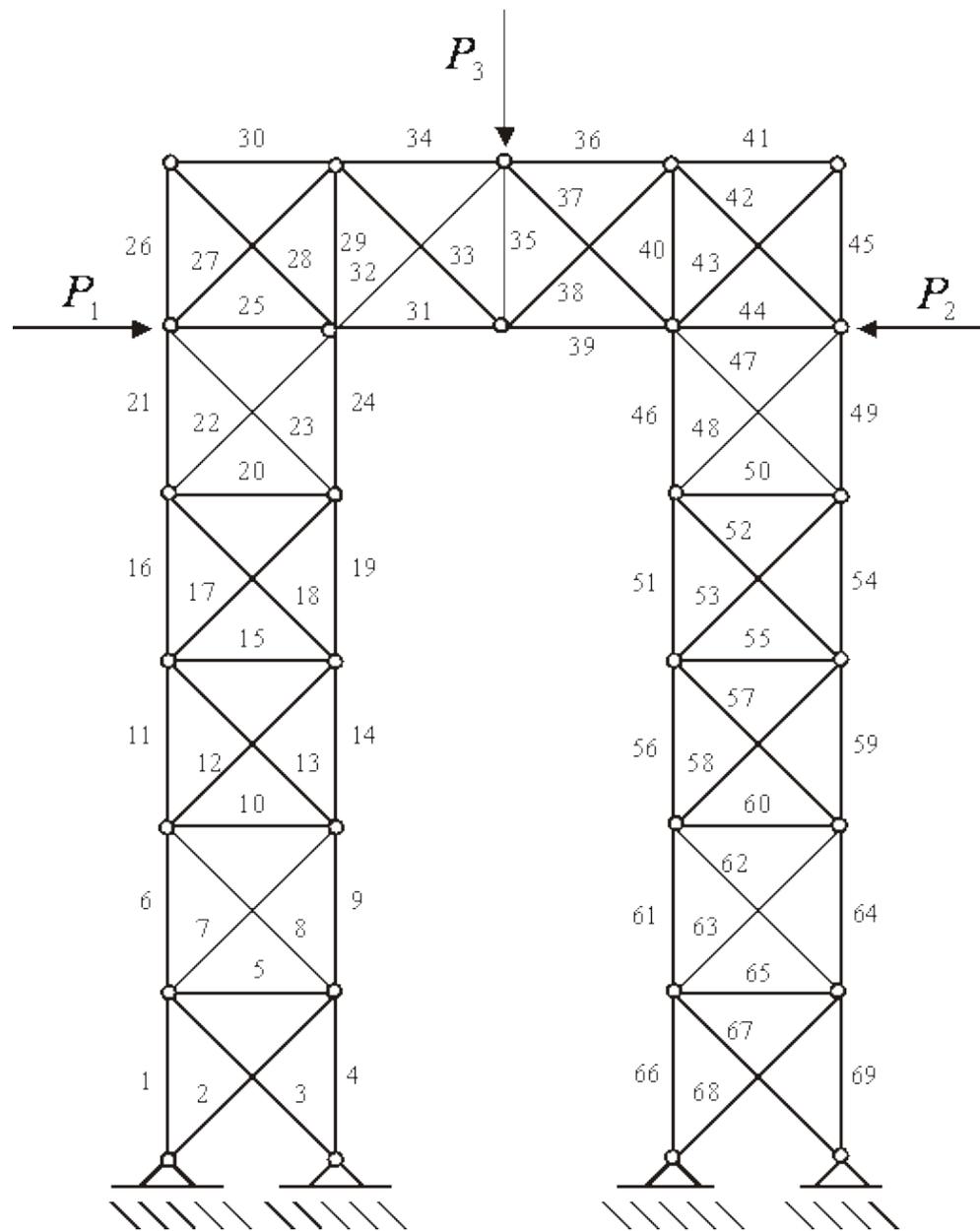
rewrite as:

$$(\check{\mathbf{A}} + \mathbf{SD})\mathbf{x} = \mathbf{b}$$

$$\left[\begin{pmatrix} \check{k} & \mathbf{C}^T \\ \mathbf{C} & \mathbf{0} \end{pmatrix} + \begin{pmatrix} \check{k} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} \end{pmatrix} \begin{pmatrix} \mathbf{d} & \mathbf{0} \\ \mathbf{0} & \mathbf{0} \end{pmatrix} \right] \begin{pmatrix} \mathbf{u} \\ \boldsymbol{\lambda} \end{pmatrix} = \begin{pmatrix} \mathbf{p} \\ \mathbf{0} \end{pmatrix}$$

Present formulation

- ▶ $\mathbf{x} = [\mathbf{u}, \boldsymbol{\lambda}]^T$, \mathbf{u} is the displacement vector
- ▶ Calculate element forces
 - Conventional FEM: $F = k u$ (overestimation)
 - Present formulation: $\mathbf{K}\mathbf{u} = \mathbf{P} - \mathbf{C}^T \boldsymbol{\lambda}$
 $\boldsymbol{\lambda} = \mathbf{L}\mathbf{x}$, $\mathbf{p} = \mathbf{M}\mathbf{b}$
 $\mathbf{P} - \mathbf{C}^T \boldsymbol{\lambda} = \mathbf{p} - \mathbf{C}^T \mathbf{L}(\mathbf{x}^{*n+1} + \mathbf{x}_0)$
 $\mathbf{P} - \mathbf{C}^T \boldsymbol{\lambda} = \mathbf{M}\mathbf{b} - \mathbf{C}^T \mathbf{L}(\mathbf{R}\mathbf{b} - \mathbf{R}\mathbf{S}\mathbf{M}^n \boldsymbol{\delta})$
 $\mathbf{P} - \mathbf{C}^T \boldsymbol{\lambda} = (\mathbf{N} - \mathbf{C}^T \mathbf{L}\mathbf{R})\mathbf{b} + \mathbf{C}^T \mathbf{L}\mathbf{R}\mathbf{S}\mathbf{M}^n \boldsymbol{\delta}$



No	Error %	No	Error %	No	Error %	No	Error %
1	107.057 %	21	42.4163 %	41	109.399 %	61	31.4828 %
2	78.991 %	22	34.0332 %	42	20.0367 %	62	95.903 %
3	38.2972 %	23	9.30111 %	43	109.399 %	63	48.1069 %
4	52.0345 %	24	100.427 %	44	0.833207 %	64	68.1526 %
5	22.7834 %	25	0.833207 %	45	116.216 %	65	22.7834 %
6	68.1526 %	26	116.216 %	46	100.427 %	66	52.0345 %
7	95.903 %	27	20.0367 %	47	34.0332 %	67	78.991 %
8	48.1069 %	28	116.216 %	48	9.30111 %	68	38.2972 %
9	31.4828 %	29	48.1793 %	49	42.4163 %	69	107.057 %
10	22.6152 %	30	116.216 %	50	15.3219 %		
11	38.0037 %	31	8.87714 %	51	33.6609 %		
12	91.4489 %	32	19.1787 %	52	119.633 %		
13	45.9704 %	33	35.7319 %	53	47.414 %		
14	11.913 %	34	18.7494 %	54	9.99375 %		
15	24.3824 %	35	6.38613 %	55	24.3824 %		
16	9.99375 %	36	18.7494 %	56	11.913 %		
17	119.633 %	37	19.1787 %	57	91.4489 %		
18	56.7357 %	38	35.7319 %	58	45.9704 %		
19	33.6609 %	39	8.87714 %	59	38.0037 %		
20	15.3219 %	40	48.1793 %	60	22.6152 %		



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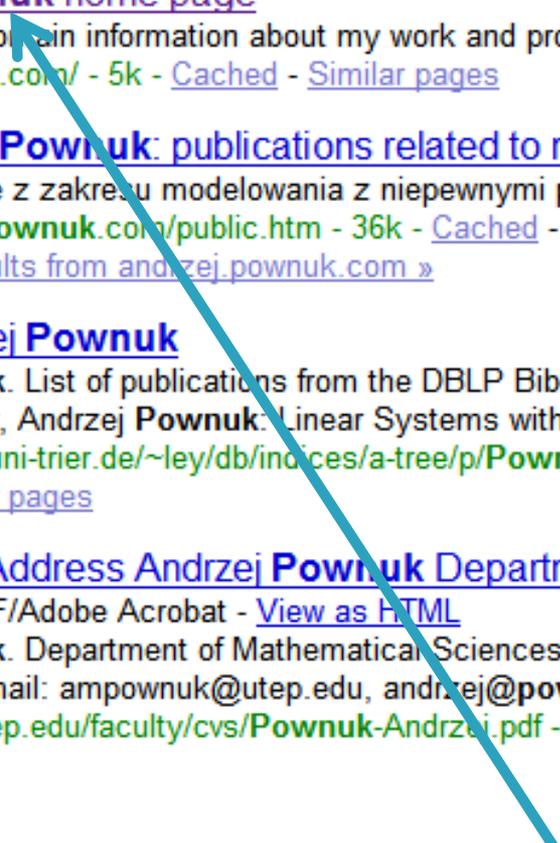
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[[Computational Science Ph.D. Program at UTEP](#)] [[Interval equations \(list of references\)](#)]



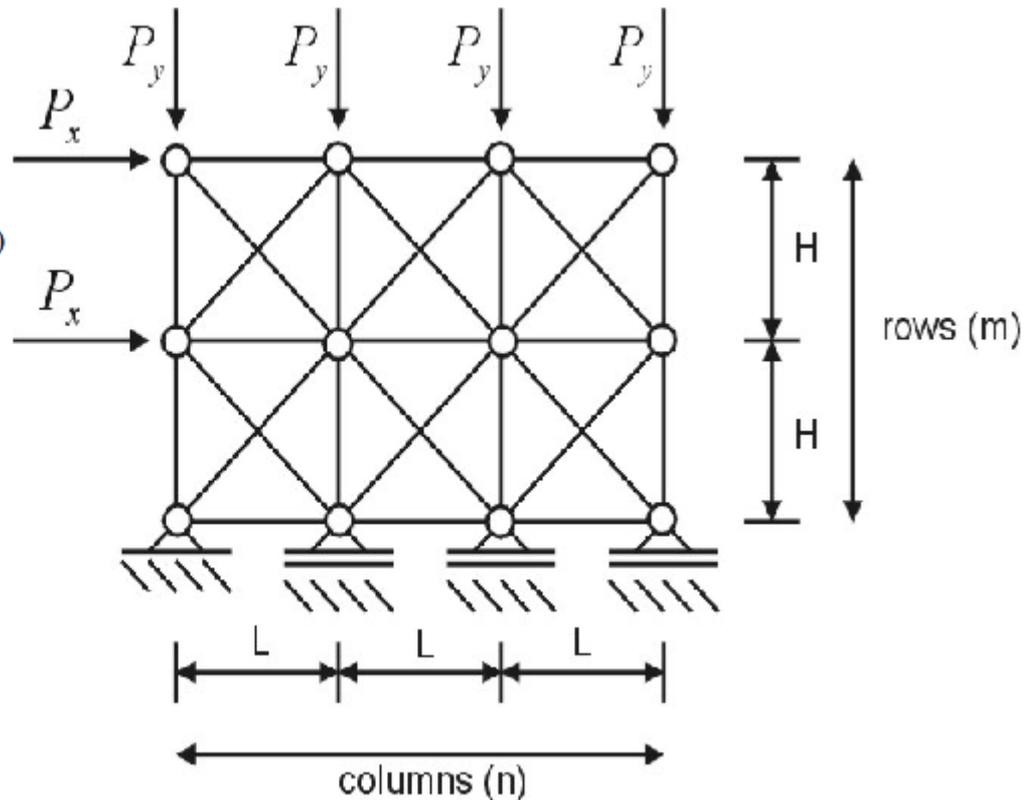
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Truss structure with interval parameters

Describe the structure

2	Number of rows (n)
3	Number of columns (m)
2	L [m]
1	H [m]
10	P _x [kN]
10	P _y [kN]
210E9	E [N/m ²]
0.0025	A [m ²]
5	dE [%]
5	dA [%]

Generate the code



Monotonicity of the solution

- ▶ Monotone solution

$$\begin{bmatrix} 1 & 1 \\ 1 & -1 \end{bmatrix} \begin{bmatrix} u_1 \\ u_2 \end{bmatrix} = \begin{bmatrix} p_1 + p_2 \\ p_2 \end{bmatrix}$$

$$u_1 = \frac{p_1}{2} + p_2, u_2 = \frac{p_1}{2}$$

$$u^2 - p^4 = 0$$

- ▶ Non-monotone solution

$$u_1 = p^2, u_2 = -p^2$$

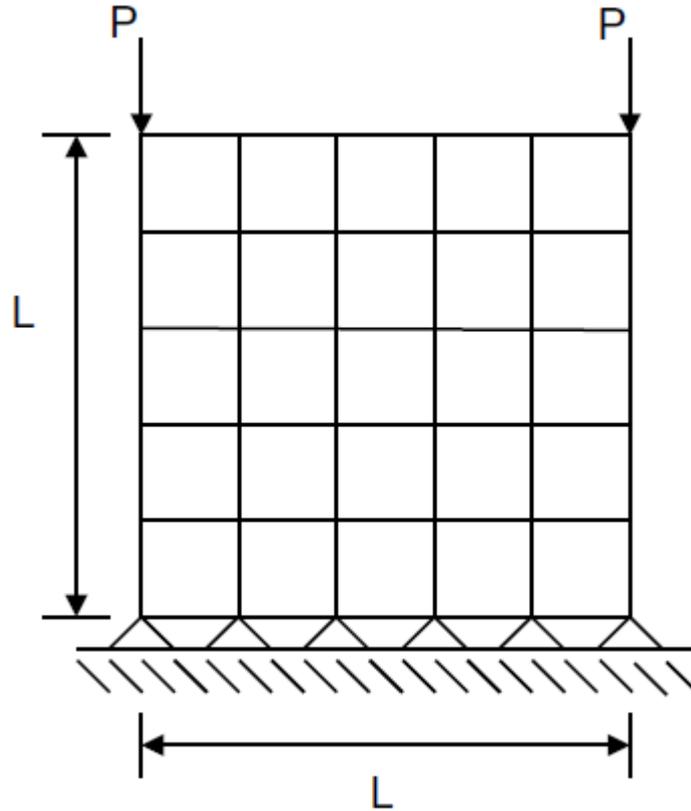
Interval solution for monotone functions (gradient descent method)

$$\text{If } \frac{\partial u}{\partial p} \geq 0 \quad \text{then} \quad p^{m \text{ in}} = \underline{p}, p^{m \text{ ax}} = \bar{p}$$

$$\text{If } \frac{\partial u}{\partial p} < 0 \quad \text{then} \quad p^{m \text{ in}} = \bar{p}, p^{m \text{ ax}} = \underline{p}$$

$$\underline{u} = u(p^{m \text{ in}}), \bar{u} = u(p^{m \text{ ax}})$$

Monotonicity of the solution



Plane stress

$$\begin{bmatrix} e_{xx} \\ e_{yy} \\ 2e_{xy} \end{bmatrix} = \begin{bmatrix} \partial/\partial x & 0 \\ 0 & \partial/\partial y \\ \partial/\partial y & \partial/\partial x \end{bmatrix} \begin{bmatrix} u_x \\ u_y \end{bmatrix},$$

$$\begin{bmatrix} \sigma_{xx} \\ \sigma_{yy} \\ \sigma_{xy} \end{bmatrix} = \begin{bmatrix} E_{11} & E_{12} & E_{13} \\ E_{12} & E_{22} & E_{23} \\ E_{13} & E_{23} & E_{33} \end{bmatrix} \begin{bmatrix} e_{xx} \\ e_{yy} \\ 2e_{xy} \end{bmatrix},$$

$$\begin{bmatrix} \partial/\partial x & 0 & \partial/\partial y \\ 0 & \partial/\partial y & \partial/\partial x \end{bmatrix} \begin{bmatrix} \sigma_{xx} \\ \sigma_{yy} \\ \sigma_{xy} \end{bmatrix} + \begin{bmatrix} b_x \\ b_y \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}.$$

Interval solution

Verification of the results by using search method with 3 intermediate points

Table VIII. Displacements in the case of 4 (2x2) finite elements and 5% uncertainty

	Combinatoric	Combinatoric	Gradient free	Gradient free		
DOF	\underline{u}	\bar{u}	\underline{u}	\bar{u}	Error \underline{u} %	Error \bar{u} %
5	-8.770130E-23	1.113670E-22	-8.770130E-23	1.113670E-22	0.000000E+00	0.000000E+00
6	-4.404760E-07	-3.605710E-07	-4.404760E-07	-3.605710E-07	0.000000E+00	0.000000E+00
7	4.822140E-08	5.890760E-08	4.822140E-08	5.890760E-08	0.000000E+00	0.000000E+00
8	-6.087950E-07	-4.983560E-07	-6.087950E-07	-4.983560E-07	0.000000E+00	0.000000E+00
11	-5.890760E-08	-4.822140E-08	-5.890760E-08	-4.822140E-08	0.000000E+00	0.000000E+00
12	-6.087950E-07	-4.983560E-07	-6.087950E-07	-4.983560E-07	0.000000E+00	0.000000E+00
13	-1.851990E-23	2.469330E-22	-1.851990E-23	2.469330E-22	0.000000E+00	0.000000E+00
14	-3.540790E-07	-2.898470E-07	-3.540790E-07	-2.898470E-07	0.000000E+00	0.000000E+00
15	-4.815970E-07	-3.942320E-07	-4.815970E-07	-3.942320E-07	0.000000E+00	0.000000E+00
16	-1.840780E-06	-1.506850E-06	-1.840780E-06	-1.506850E-06	0.000000E+00	0.000000E+00
17	3.942320E-07	4.815970E-07	3.942320E-07	4.815970E-07	0.000000E+00	0.000000E+00
18	-1.840780E-06	-1.506850E-06	-1.840780E-06	-1.506850E-06	0.000000E+00	0.000000E+00

Interval solution

Table X. Displacements in the case of 9 (3x3) finite elements and 5% uncertainty

	Combinatoric		Gradient free			
DOF	\underline{u}	\bar{u}	\underline{u}	\bar{u}	Error \underline{u} %	Error \bar{u} %
5	2.991120E-09	4.758950E-08	2.991120E-09	4.758950E-08	0.000000E+00	0.000000E+00
6	-3.401560E-07	-2.737550E-07	-3.401560E-07	-2.738240E-07	0.000000E+00	2.520502E-02
7	-2.700300E-08	3.178720E-08	-2.681040E-08	3.178720E-08	7.132541E-01	0.000000E+00
8	-4.259370E-07	-2.781400E-07	-4.259370E-07	-2.781400E-07	0.000000E+00	0.000000E+00
11	-4.758950E-08	-2.991120E-09	-4.758950E-08	-2.991120E-09	0.000000E+00	0.000000E+00
12	-3.401560E-07	-2.737550E-07	-3.401560E-07	-2.738240E-07	0.000000E+00	2.520502E-02
15	-3.178720E-08	2.700300E-08	-3.178720E-08	2.681040E-08	0.000000E+00	7.132541E-01
16	-4.259370E-07	-2.781400E-07	-4.259370E-07	-2.781400E-07	0.000000E+00	0.000000E+00
17	-8.584880E-09	1.665680E-07	-8.584880E-09	1.665680E-07	0.000000E+00	0.000000E+00
18	-5.498820E-07	-4.324890E-07	-5.498820E-07	-4.324890E-07	0.000000E+00	0.000000E+00

Interval solution

Table XI. Combinations of parameters which correspond to the interval displacements 9 elements (3x3) and 5% uncertainty

	Combinatoric	Combinatoric	Gradient free	Gradient free		
DOF	\underline{u}	\bar{u}	\underline{u}	\bar{u}	\underline{u}	\bar{u}
5	0,1,1,0,1,0,1,1,1,0,1	1,0,0,1,0,1,0,0,0,1,0	0,1,1,0,1,0,1,1,1,0,1	1,0,0,1,0,1,0,0,0,1,0	0	0
6	0,0,0,0,1,0,1,1,1,0,1	1,1,1, $\boxed{0}$,0,1,0,0,0,1,0	0,0,0,0,1,0,1,1,1,0,1	1,1,1, $\boxed{1}$,0,1,0,0,0,1,0	0	1
7	0,0,1,0,1,0,1,1,1,0,1	1, $\boxed{0}$,0,1,0,1,0,0,0,1,0	0, $\boxed{1}$,1,0,1,0,1,1,1,0,1	1,0,0,1,0,1,0,0,0,1,0	1	0
8	0,0,1,1,0,1,0,0,0,0,1	1,1,0,0,1,0,1,1,1,1,0	0,0,1,1,0,1,0,0,0,0,1	1,1,0,0,1,0,1,1,1,1,0	0	0
11	0,0,1,1,0,1,0,0,0,0,1	1,1,0,0,1,0,1,1,1,1,0	0,0,1,1,0,1,0,0,0,0,1	1,1,0,0,1,0,1,1,1,1,0	0	0
12	0,0,0,0,1,0,1,1,1,1,0	1,1,1,1,0, $\boxed{0}$,0,0,0,0,1	0,0,0,0,1,0,1,1,1,1,0	1,1,1,1,0, $\boxed{1}$,0,0,0,0,1	0	1
15	0,0,1,1,0,1,0,0,0,0,1	1, $\boxed{0}$,0,0,1,0,1,1,1,1,0	0,0,1,1,0,1,0,0,0,0,1	1, $\boxed{1}$,0,0,1,0,1,1,1,1,0	0	1
16	1,0,0,1,0,1,0,0,0,1,0	0,1,1,0,1,0,1,1,1,0,1	1,0,0,1,0,1,0,0,0,1,0	0,1,1,0,1,0,1,1,1,0,1	0	0
17	0,1,1,1,1,1,0,1,0,0,1	1,0,0,0,0,0,1,0,1,1,0	0,1,1,1,1,1,0,1,0,0,1	1,0,0,0,0,0,1,0,1,1,0	0	0
18	0,0,0,0,0,0,1,1,1,0,1	1,1,1,1,1,1,0,0,0,1,0	0,0,0,0,0,0,1,1,1,0,1	1,1,1,1,1,1,0,0,0,1,0	0	0

Interval solution

Table XII. Interval displacements for 10% uncertainty and 9 finite elements

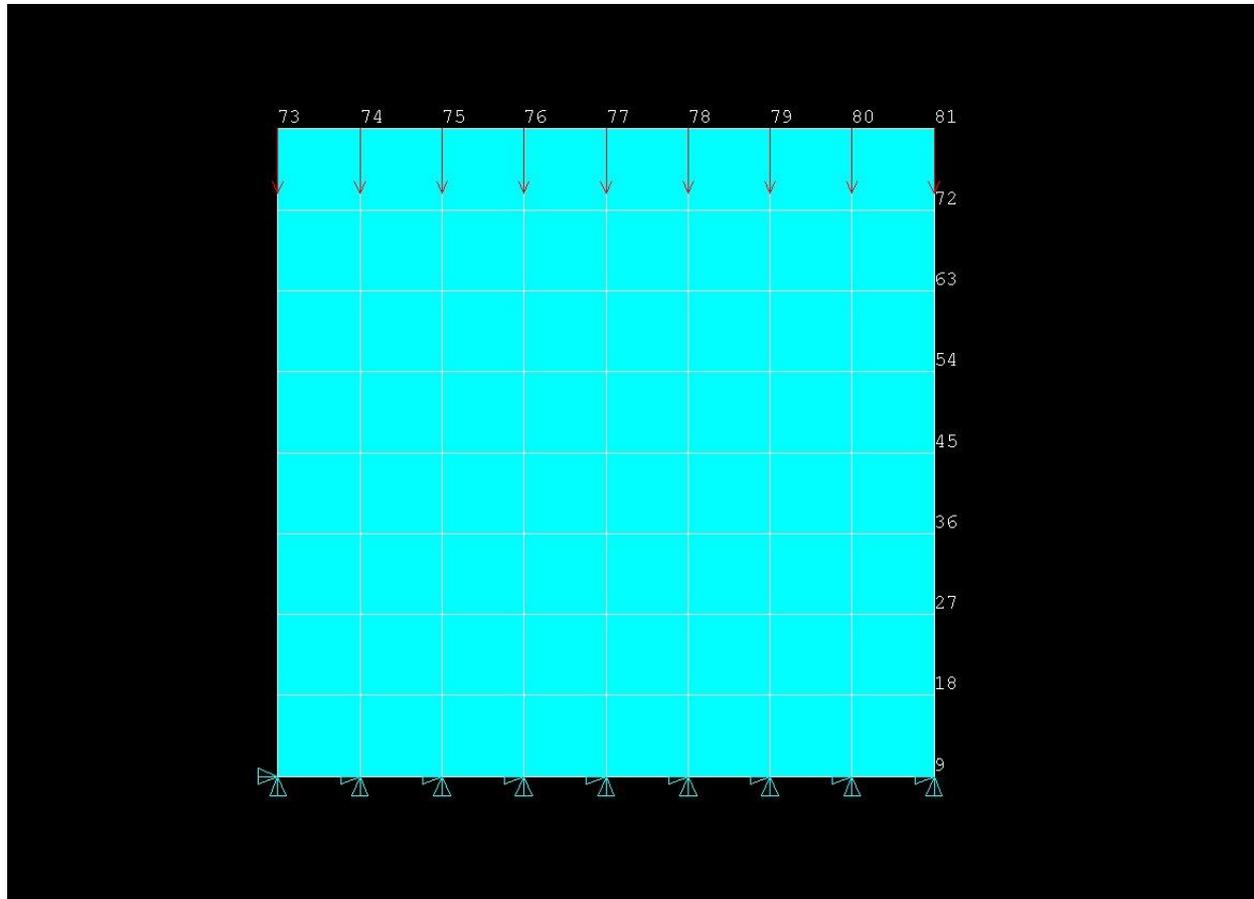
DOF	\underline{u}	\bar{u}	\underline{u}	\bar{u}	Error \underline{u} %	Error \bar{u} %
5	-1.934900E-08	7.022680E-08	-1.934900E-08	7.022470E-08	0.000000E+00	2.990311E-03
6	-3.796920E-07	-2.451030E-07	-3.796920E-07	-2.458330E-07	0.000000E+00	2.978340E-01
7	-5.781790E-08	6.089000E-08	-5.677190E-08	6.089000E-08	1.809128E+00	0.000000E+00
8	-5.089660E-07	-2.112750E-07	-5.089660E-07	-2.112750E-07	0.000000E+00	0.000000E+00
11	-7.022680E-08	1.934900E-08	-7.022470E-08	1.934900E-08	2.990311E-03	0.000000E+00
12	-3.796920E-07	-2.451030E-07	-3.796920E-07	-2.458330E-07	0.000000E+00	2.978340E-01
15	-6.089000E-08	5.781790E-08	-6.089000E-08	5.677190E-08	0.000000E+00	1.809128E+00
16	-5.089660E-07	-2.112750E-07	-5.089660E-07	-2.112750E-07	0.000000E+00	0.000000E+00
17	-9.469690E-08	2.590120E-07	-9.315200E-08	2.590120E-07	1.631416E+00	0.000000E+00
18	-6.187590E-07	-3.820950E-07	-6.187590E-07	-3.820950E-07	0.000000E+00	0.000000E+00

Interval solution

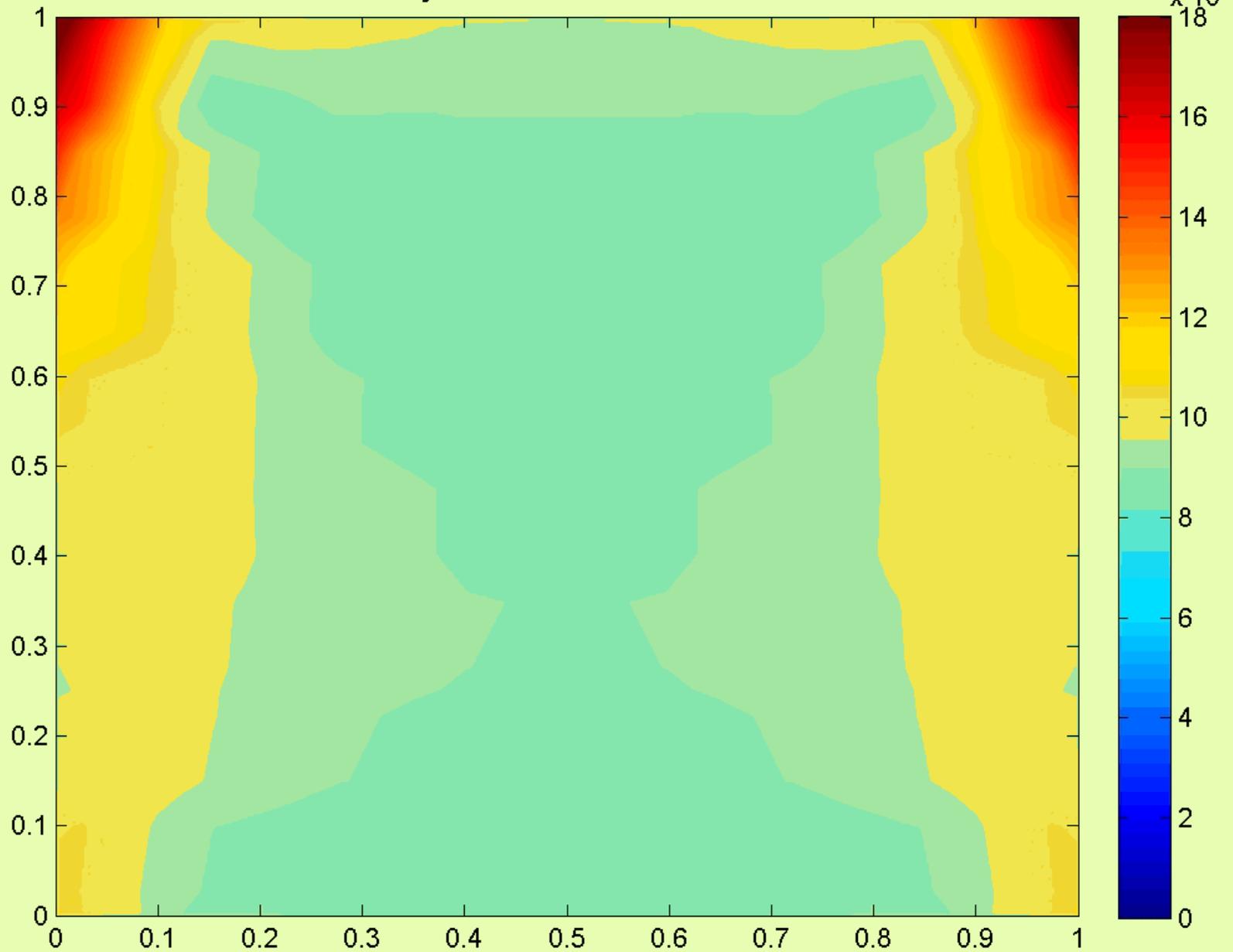
Table XV. Interval displacements 10% uncertainty

\underline{u}	\bar{u}	\underline{u}	\bar{u}		
0,1,1,0,1,0,1,1,1,0,1	1,0,0,1,0,1,1,0,0,1,0	0,1,1,0,1,0,1,1,1,0,1	1,0,0,1,0,1,0,0,0,1,0	0	1
0,0,0,0,1,0,1,1,1,0,1	1,1,1,0,0,1,0,0,0,1,0	0,0,0,0,1,0,1,1,1,0,1	1,1,1,0,0,1,0,0,0,1,0	0	1
0,0,1,0,1,0,1,1,1,0,1	1,0,0,1,0,1,0,0,0,1,0	0,1,0,1,0,1,1,1,0,1	1,0,0,1,0,1,0,0,0,1,0	1	0
0,0,1,1,0,1,0,0,0,0,1	1,1,0,1,1,0,1,1,1,1,0	0,0,1,1,0,1,0,0,0,0,1	1,1,0,1,1,0,1,1,1,1,0	0	0
0,0,1,1,0,1,0,0,1,0,1	1,1,0,0,1,0,1,1,0,1,0	0,0,1,1,0,1,0,0,0,0,1	1,1,0,0,1,0,1,1,1,1,0	1	0
0,0,0,0,1,0,1,1,1,1,0	1,1,1,1,0,0,0,0,0,0,1	0,0,0,0,1,0,1,1,1,1,0	1,1,1,1,0,0,0,0,0,0,1	0	1
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0,1,1,1,1,1,0,0,0,0,1	1,0,0,0,0,0,1,1,1,1,0	0,1,1,1,1,1,0,0,0,0,1	1,0,0,0,0,0,1,1,1,1,0	0	0
0,0,1,0,0,1,0,0,0,0,1	1,1,0,1,1,0,1,1,1,1,0	0,0,1,0,0,1,0,0,0,0,1	1,1,0,1,1,0,1,1,1,1,0	0	0
0,0,1,0,0,0,1,0,1,0,1	1,0,0,1,1,0,0,1,0,1,0	0,0,1,0,0,0,1,0,1,0,1	1,0,0,1,1,0,1,0,1,0,1	0	2

2D problem with the internal parameters and interval functions parameters



uncertainty = 5% min= 82711 max= 188847



Scripting language

```
analysis_type linear_static_functional_derivative
```

```
parameter 1 [210E9,212E9] # E  
parameter 2 [0.2,0.4] # Poisson number  
parameter 3 0.1 # thickness  
parameter 4 [-3,-1] sensitivity # fy
```

```
point 1 x 0 y 0  
point 2 x 1 y 0  
point 3 x 1 y 1  
point 4 x 0 y 1  
point 5 x -1 y 0  
point 6 x -1 y 1
```

```
rectangle 1 points 1 2 3 4 parameters 1 2 3  
rectangle 2 points 5 1 4 6 parameters 1 2 3
```

```
load constant_distributed_in_y_local_direction  
geometrical_object 1 fy 4  
load constant_distributed_in_y_local_direction  
geometrical_object 2 fy 4
```

```
boundary_condition fixed point 1 ux  
boundary_condition fixed point 1 uy  
boundary_condition fixed point 2 ux  
boundary_condition fixed point 2 uy  
boundary_condition fixed point 5 ux  
boundary_condition fixed point 5 uy
```

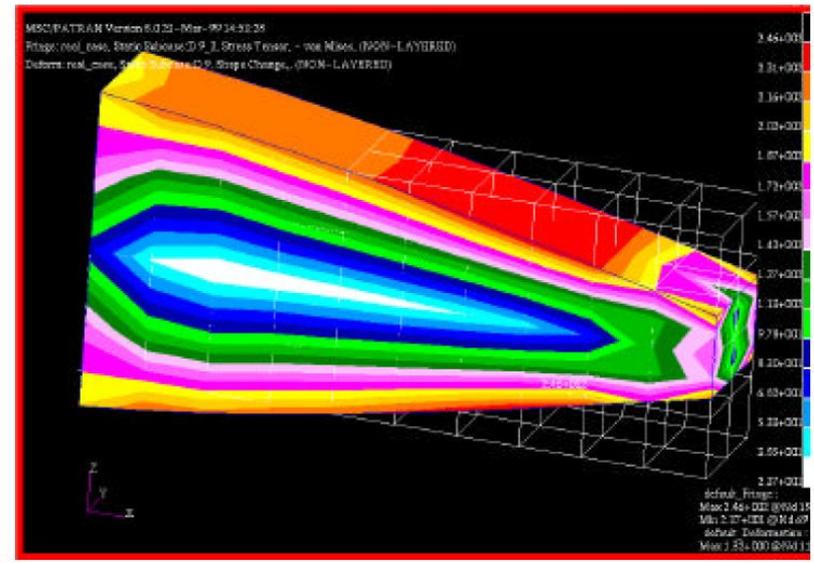
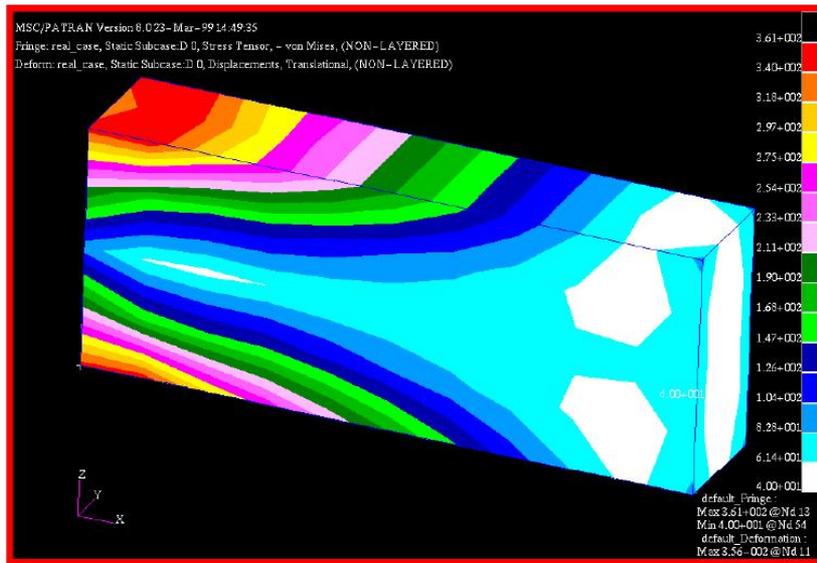
```
#Mesh
```

Shape optimization

$$\begin{cases} \min u = u(\Omega) \\ \Omega \in [\underline{\Omega}, \bar{\Omega}] \end{cases}$$

or

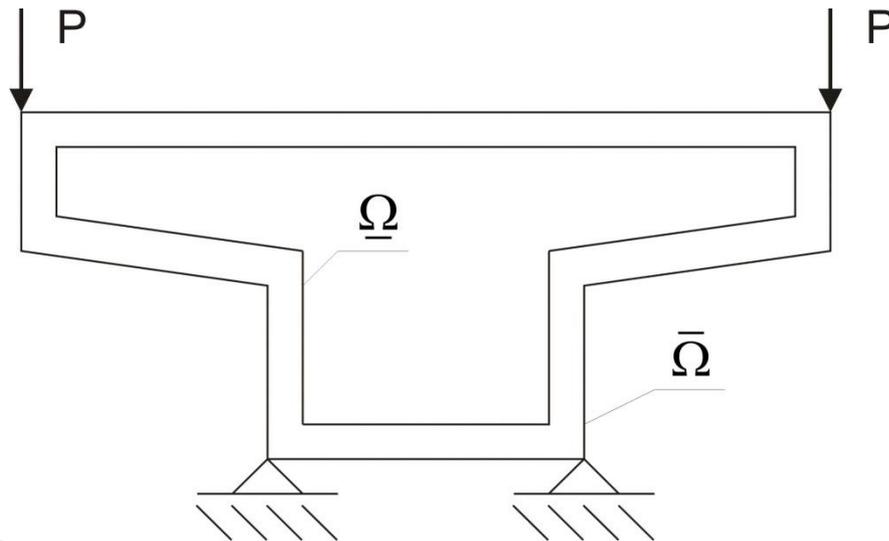
$$\begin{cases} \min u = u(\Omega) \\ C(\Omega) = 0 \\ \Omega \in [\underline{\Omega}, \bar{\Omega}] \end{cases}$$



Interval set

$$A \leq B \Leftrightarrow A \subseteq B$$

$$\mathbf{\Omega} = [\underline{\Omega}, \bar{\Omega}] = \{ \Omega : \underline{\Omega} \leq \Omega \leq \bar{\Omega} \}$$



Set dependent functions

Center of gravity

$$x_C(\Omega) = \frac{\int x d\mu}{\int_{\Omega} d\mu}$$

Moment of inertia

$$I(\Omega) = \int_{\Omega} y^2 d\mu$$

Solution of PDE

$$\begin{cases} \Delta u + q = \frac{\partial u}{\partial t} & \text{for } x \in \text{int } \Omega \\ u = u^* & \text{for } x \in \partial\Omega \end{cases}$$

Topological derivative

$$\lim_{\rho(\Delta\Omega) \rightarrow 0^+} \frac{u(\Omega + \Delta\Omega) - u(\Omega)}{f(\Delta\Omega)} = \lim_{\varepsilon \rightarrow 0} \frac{\frac{du}{d\varepsilon}}{\frac{df}{d\varepsilon}} = D_T(x)$$

Topological derivative

Examples

$$f(\Omega) = \int_{\Omega} L(x) d\mu$$

$$\frac{df(\Omega)}{d\mu} = L(x)$$

$$x_c(\Omega) = \frac{\int_{\Omega} x d\mu}{\int_{\Omega} d\mu}$$

$$\frac{dx_c(\Omega)}{d\mu} = \frac{x|\Omega| - \int_{\Omega} x d\mu}{\left(\int_{\Omega} d\mu\right)^2}$$

Extreme values of monotone functions

$$f(x) = x^2, \quad x \in [1, 2]$$

$$\frac{df(x)}{dx} = 2x \in [2, 4]$$

$$\underline{f} = f(\underline{x}) = 1^2 = 1$$

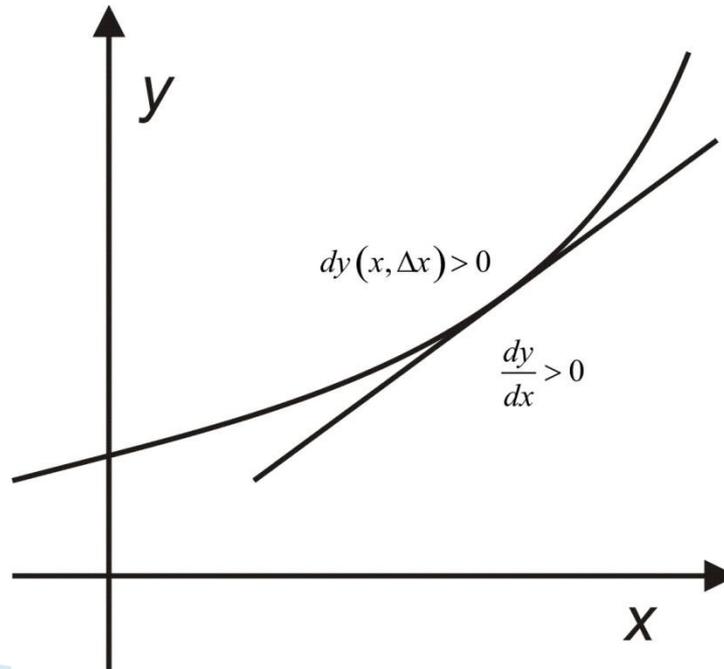
$$\bar{f} = f(\bar{x}) = 2^2 = 4$$

$$f(x) \in [\underline{f}, \bar{f}] = [1, 4]$$

Topological derivative and monotonicity

$$f(\Omega + \Delta\Omega) - f(\Omega) \approx df(\Omega, \Delta\Omega) \geq 0$$

$$f(\Omega + \Delta\Omega) \geq f(\Omega)$$



Parametric representation

$$\lim_{\varepsilon \rightarrow 0^+} \frac{u(\Omega_\varepsilon) - u(\Omega)}{f(\varepsilon)} = \lim_{\varepsilon \rightarrow 0} \frac{\frac{du}{d\varepsilon}}{\frac{df}{d\varepsilon}}$$

Results which are independent of parameterization

$$f(\Omega) = \left(\int_{\Omega} L(x) d\mu \right)^2$$

$$f(\Omega + \Delta\Omega) - f(\Omega) \approx 2 \left(\int_{\Omega} L(x) d\mu \right) L(x) |\Delta\Omega|$$

Results which are dependent on parameterization

$$\Omega = [x_0, x_1] \subset R$$

$$f(\Omega) = \frac{x - x_0}{x_1 - x_0} \qquad |\Omega| = |x_1 - x_0|$$

$$\frac{df}{d\mu} = \lim_{\Delta x_1 \rightarrow 0^+} \frac{f(x_1 + \Delta x_1) - f(x_1)}{|\Omega(x_1 + \Delta x_1)| - |\Omega(x_1)|} = \frac{\frac{df}{dx_1}}{\frac{d\Omega}{dx_1}} = -\frac{x - x_0}{(x_1 - x_0)^2}$$

Results which are dependent on parameterization

$$f(\Omega) = \frac{x - x_0}{x_1 - x_0} \qquad |\Omega| = |x_1 - x_0|$$

$$\frac{df}{d\mu} = \lim_{\Delta x_0 \rightarrow 0^+} \frac{f(x_0 + \Delta x_0) - f(x_0)}{|\Omega(x_0 + \Delta x_0)| - |\Omega(x_0)|} = \frac{\frac{df}{dx_0}}{\frac{d\Omega}{dx_0}} = \frac{x - x_1}{(x_1 - x_0)^2}$$

$$\frac{\frac{df}{dx_1}}{\frac{d\Omega}{dx_1}} \neq \frac{\frac{df}{dx_0}}{\frac{d\Omega}{dx_0}}$$

Computational method

Formulation of the problem

$$K(p)u = Q(p)$$

$$f(p) = |\Omega(p)|$$

Calculation of the derivative

$$K(p) \frac{\partial u}{\partial p} = \frac{\partial Q(p)}{\partial p} - \frac{\partial K(p)}{\partial p} u$$

$$\frac{\partial f(p)}{\partial p} = \frac{\partial |\Omega(p)|}{\partial p}$$

Computational method

$$\frac{\partial u}{\partial \Omega} = \frac{\frac{\partial u}{\partial p}}{\frac{\partial p}{\partial \Omega}}$$

If $du(\Omega, \Delta\Omega) \geq 0$ then $\Omega_{i+1} = \Omega_i + \Delta\Omega$

If $du(\Omega, \Delta\Omega) < 0$ then $\Omega_{i+1} = \Omega_i - \Delta\Omega$

for $x \in \partial\Omega$

Data for Calculations

- ▶ Coordinates of the nodes are the interval numbers.

$$x_i \in [\underline{x}_i, \bar{x}_i]$$

- ▶ Loads, material parameters (E, ν) can be also the interval numbers.

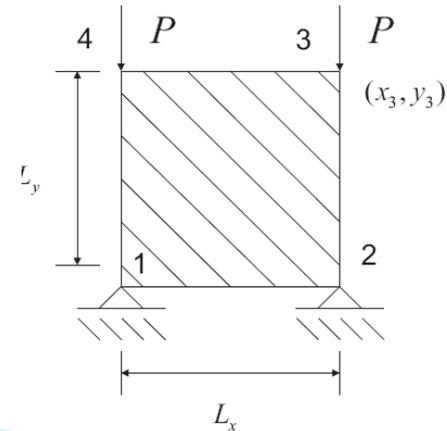
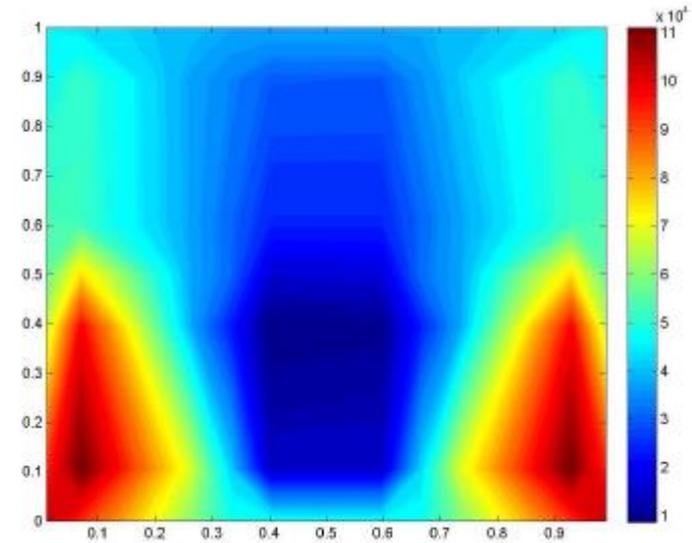
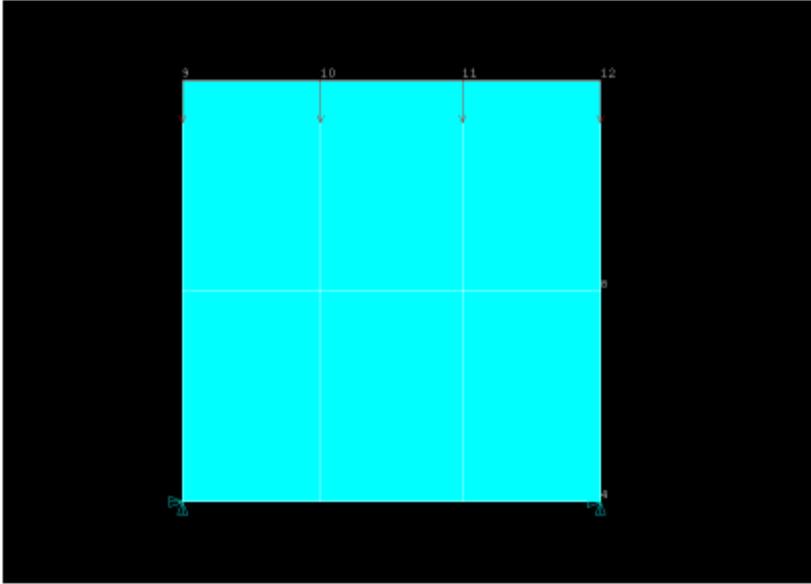
$$P \in [\underline{P}, \bar{P}], E \in [\underline{E}, \bar{E}], \nu \in [\underline{\nu}, \bar{\nu}]$$

Interval solution

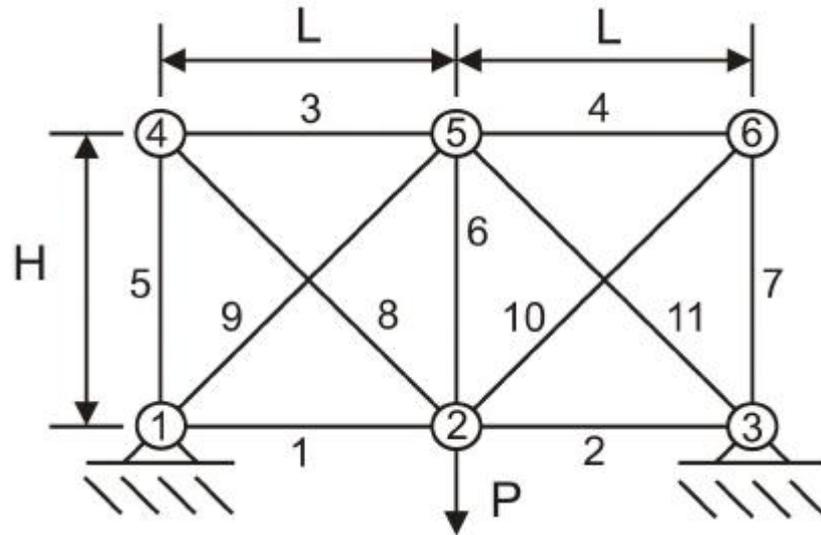
$$\mathbf{u}(x) = \diamond \{u(x, \Omega) : \Omega \in [\underline{\Omega}, \bar{\Omega}]\}$$

$$\underline{u}(x) = u(x, \Omega^{m \text{ in}}), \quad \bar{u}(x) = u(x, \Omega^{m \text{ ax}})$$

Interval von Mises stress



Truss structure with the uncertain geometry



	Lower bound [m]	Upper bound [m]
u_{2x}	-2.883822e-005	2.886680e-005
u_{2y}	-1.526831e-002	-1.463698e-002
u_{5x}	-7.216225e-005	7.214392e-005
u_{5y}	-1.296921e-002	-1.239865e-002

Conclusions

- ▶ Current civil engineering codes are based on worst case design concept, because of that it is possible to use presented approach in the framework of existing law.
 - ▶ Using presented method it is possible to solve engineering problems with interval parameters (interval parameters, functions, sets).
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